



Primary & Secondary Composite Wall Materials

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Overview

- Review of shielding materials & their properties
- Lead/concrete primary barriers – low energy
- Lead/concrete primary barriers – high energy
- Secondary barriers
- Practical considerations
- Composite doors
- Escape hatch
- “Source constraints”

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Shielding Materials

Materials	Density (g/cm ³)	Comments
Concrete	2.35; 3.85	High density concrete is very expensive
Concrete blocks	2.35; 3.85; 4.62	Lack structural integrity of concrete
Lead	11.35	Great for photons; bad for neutrons. Needs structural support
Steel	7.87	Not as efficient as lead for photons
Earth	1.5	Cheap! Build underground
Brick	1.65 - 2.05	
Polyethylene; borated polyethylene	~1.0	Used to shield against neutrons in doors, ducts etc.

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Tenth Value Layers

<u>Primary TVLs (cm)*</u>						
Energy (MV)	4	6	10	15	18	20
Concrete	35(30)	37(33)	41(37)	44(41)	45(53)	46(44)
Steel	9.9	10	11	11	11	11
Lead	5.7	5.7	5.7	5.7	5.7	5.7

<u>Leakage TVLs (90°)*</u>						
Energy (MV)	4	6	10	15	18	20
Concrete	33(28)	34(29)	35(31)	36(33)	36(34)	36(34)
Steel**		8	8.5	8.7	8.7	
Lead**		4.5	4.6	4.7	4.7	

* First term is 1st TVL and term in brackets is for all other TVLs.
Data from NCRP #151
** Data from McGinley

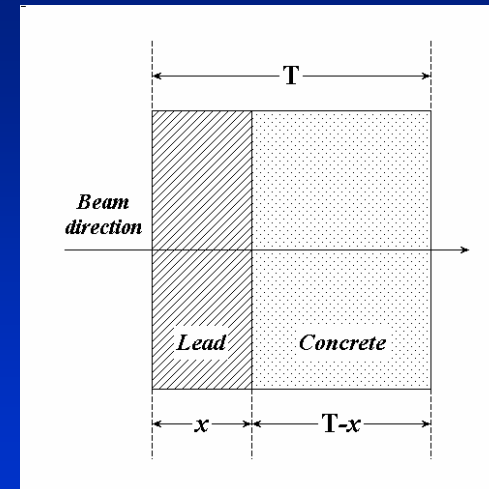
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Rationale for Laminated shielding

- upgrading existing facilities from low energy to high energy
- remodelling existing facilities where space is limited
- new facilities where space is limited
- requires high density, high-Z material
- photoneutron production, capture γ rays for high energy beams

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Geometry for Laminate Problem



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Laminated Barriers I: Low Energy

The general equations to determine the relative (optimal) thicknesses of lead and concrete for a single energy x-ray beam (no neutrons) for a fixed wall thickness are:

$$n_T = n_c + n_l$$
$$T = n_c TVL_c + n_l TVL_l$$

where n_T is the total number of TVLs, T is the overall thickness and c and l refer to concrete and lead respectively.

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Laminated Barriers II

The solution to these equations is:

$$n_l = \frac{n_T TVL_c - T}{TVL_c - TVL_l}$$
$$n_c = n_T - n_l$$

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Laminated Barriers II

However, life under NCRP #151 is not quite so simple since there are now two TVLs for concrete, so the equations become:

$$n_T = n_c + n_l$$
$$T = TVL_{c,1} + (n_c - 1)TVL_{c,e} + n_l TVL_l$$

where $(c,1)$, is the first TVL and (c,e) are the subsequent TVLs for concrete.

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Laminated Barriers III

The solution to these equations is:

$$n_c = \frac{n_T TVL_{c,e} - T + (TVL_{c,1} - TVL_{c,e})}{TVL_{c,e} - TVL_l}$$
$$n_l = n_T - n_c$$

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Laminated Barriers IV

However, if lead is the first material in the beamline and the thickness is > 1 TVL, then only TVL_{c,e} is needed and the equations become:

$$n_T = n_c + n_l$$
$$T = n_c TVL_{c,e} + n_l TVL_l$$

with the solution

$$n_l = \frac{n_T TVL_{c,e} - T}{TVL_{c,e} - TVL_l}$$

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Example

- Assume that a maximum thickness of 122 cm (48") is specified for the primary barrier thickness, that $W=750$ Gy/wk; $d=7$ m; $U=0.213$; $T=1$; $P=0.02$ mSv/wk. One calculates $n_T = 5.2$.
- For a 15 MV x-ray beam: $TVL_{c,e} = 41$ cm and $TVL_l = 5.7$ cm
- $\therefore n_l = 2.6$, so $t_l = 14.7$ cm (5.8")
- $\therefore n_c = 2.6$, so $t_c = 107.3$ cm (42.2")

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Mixed Energy Beams I

- The majority of radiotherapy units sold today are dual energy machines
- Virtually all radiotherapy centers use a mix of photon energies
- If one uses 6 MV for IMRT, as many centers do, the majority of MU delivered could be at low energy
- Example: At MGH, for a 6/18 MV machine the energy use prior to IMRT was 20%/80% (MU). With 28% IMRT patient load, the use was 70%/30%

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Mixed Energy Beams II

- The equations now become more complicated (assuming lead is the first material and ignoring neutrons):

$$P_T = P_6 + P_{10} = \frac{UT}{d^2} \left(W_6 * 10^{\frac{(T-x)}{TVL_{c,e,6}}} * 10^{\frac{x}{TVL_{l,6}}} + W_{10} * 10^{\frac{(T-x)}{TVL_{c,e,10}}} * 10^{\frac{x}{TVL_{l,10}}} \right)$$

- This equation is solved using an iterative procedure or by solving separately for the two energies and making the usual comparison (<1TVL difference, add 1 HVL)

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Mixed Energy Beams III

- One can take the alternative approach of using only the highest energy to calculate the primary and the mixed energies to calculate the leakage (90°) radiation.
- The rationale is that this represents the worst case for both the primary (higher energy) and the leakage (higher MU)

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Example

- Assuming the same maximum thickness of 122 cm (48") for the primary barrier thickness, that $W_{15}=225$ Gy/wk; $W_6=525$ Gy; $d=7$ m; $U=0.213$; $T=1$; $P=0.02$ mSv/wk.
- For a 15 MV x-ray beam: $TVL_{c,e} = 41$ cm and $TVL_l = 5.7$ cm
 - $t_l = 12.7$ cm (5")
 - $t_c = 109.2$ cm (43")

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Laminated Shielding for Secondary Barriers

Adjacent to primary:

- There are two TVLs for scattered radiation in lead
- The leakage TVLs are only for 90°
- There are no scatter TVLs for steel

90° barrier:

- Only leakage is important, particularly if IMRT is a consideration

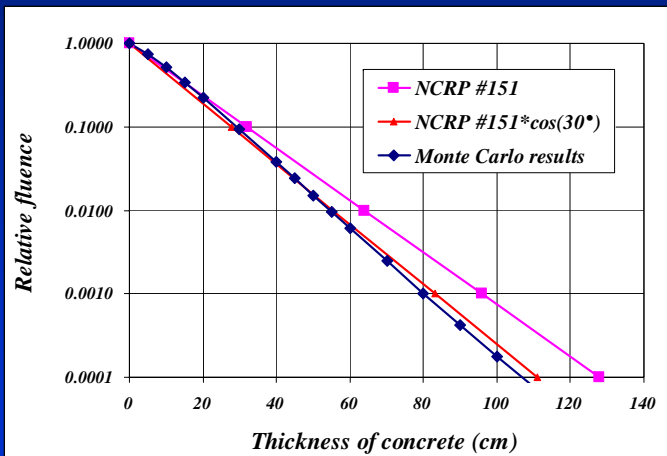
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Does the Obliquity Factor Apply to Scattered Radiation?

- Recommendations of NCRP #49 and NCRP #151
- Verify with Monte Carlo program
- Sheikh-Bagheri D. and Rogers DWO. “Monte Carlo calculation of nine megavoltage photon beam spectra using the BEAM code” *Med. Phys* 29: 391- 402; 2002

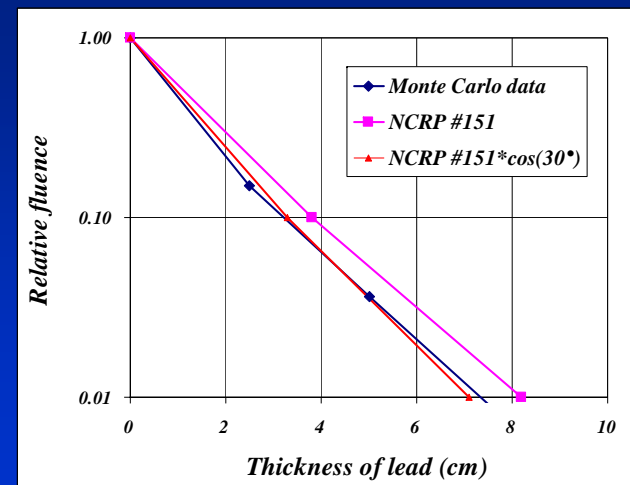
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Obliquity Factor for 30° Scattered Radiation on Concrete: 18 MV



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Obliquity Factor for 30° Scattered Radiation on Lead: 6 MV



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Re-retrofit: A Case Study

- Treatment room began operating with a Co-60 unit (Theratron 780-with beam stopper)
- This unit was replaced with a 4 MV linac with no beam stopper
- It is now being replaced with a 6 MV machine
- The first room was all regular density concrete
- The first change added lead on 3 walls plus the ceiling (to be shown on later slides)
- The current change is to add additional lead
- **Secondary barrier considerations**

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Laminated Barriers – High Energy

- *For high energy x-ray beams, neutrons have to be shielded against as well as photons*
- *For concrete-only walls, this generally presents no problem*
- *However, for laminated primary barriers, the sufficiency of the concrete barrier to protect against neutrons needs to be examined*

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Laminated shielding: Neutrons + Photons I

- The equations for determining the lead and concrete thicknesses are the same, with the constraint that the concrete is sufficient for the neutrons from the machine

$$\begin{aligned}n_{\gamma} &= n_{\gamma,c} + n_{\gamma,l} \\n_n &= n_{n,c} \\T &= n_{\gamma,c} TVL_{c,e} + n_{\gamma,l} TVL_l \\T_n &= n_n TVL_{n,c} \\with T_n &\leq n_{\gamma,c} TVL_{c,e}\end{aligned}$$

- Ignore for the moment photoproduction of neutrons and subsequent generation of capture gamma rays

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Laminated shielding: Neutrons + Photons II

- If the concrete thickness is inadequate for neutrons, then polyethylene can partially be used, so we have a new set of equations

$$\begin{aligned}n_{\gamma} &= n_{\gamma,c} + n_{\gamma,l} \\n_n &= n_{n,c} + n_{n,p} \\T &= n_{\gamma,c} TVL_{c,e} + n_{\gamma,l} TVL_l + n_{n,p} TVL_{n,p} \\T_n &= n_{n,c} TVL_{n,c} + n_{n,p} TVL_{n,p} \\with n_{n,c} TVL_{n,c} &\leq n_{\gamma,c} TVL_{c,e}\end{aligned}$$

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Laminated Barriers – High Energy

- In addition, photoneutron production in the lead and subsequent production of capture gamma rays needs to be addressed
- The greater the thickness of lead required, the greater the neutron fluence and production of capture gamma rays will be
- The magnitude of this effect will also depend how much concrete is placed after the lead

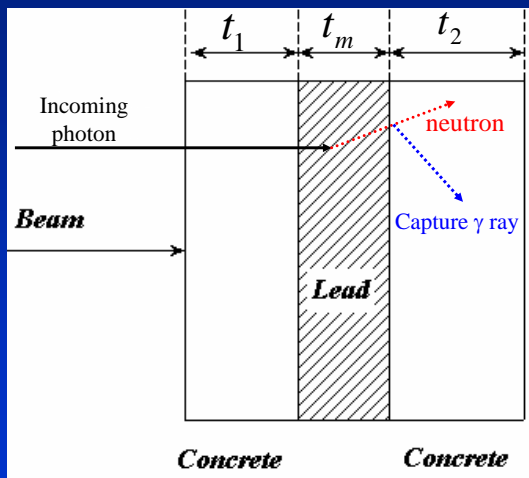
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Laminated Barriers – High Energy

- For walls, it is easy to install the lead on the upstream side of the beam since the lead can be installed in a self-supporting manner
- This is not true for shielding in the ceiling where a base support for the lead of approximately 18" concrete is required
- It also does not apply to the situation where there are two adjacent high-energy rooms facing each other where the high Z material should be centered in the concrete

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Production of Neutrons by Primary Beam in a Laminated Barrier



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Production of Neutrons by Primary Beam in a Laminated Barrier

$$H = \frac{D_0 R F_{\max}}{\left(\frac{t_m}{2} + t_2 + 0.3\right)} * 10^{-t_1/TVL_x} * 10^{-t_2/TVL_n}$$

P. McGinley

where H is the neutron dose equiv. ($\mu\text{Sv s}^{-1}$)

D_0 is the x-ray dose at isocenter (cGy s^{-1})

R is the neutron prodⁿ. rate ($\mu\text{Sv cGy}^{-1} \text{m}^{-2}$)

and F_{\max} is the max. beam area at isocenter (m^2)

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Production of Neutrons by Primary Beam in a Laminated Barrier

Note that the value of H in McGinley's equation is a balance between attenuation of the incoming photons (1st exponential term) and the attenuation of the photoproduced neutrons (2nd exponential term)

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Capture Gamma Rays

To account for capture gamma rays, NCRP recommends using a factor of 2.7 for the photon component:

$$H_{Tot} = H_n + H_{photon} = H_n + 2.7 * H_{tr}$$

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Solution to the Laminated Barrier Problem for High Energies: Two Solutions

1 Successive approximation:

- Calculate lead and concrete thicknesses required for stopping photons and concrete for neutrons separately.
- Determine dose equivalent for photon neutrons.
- Determine overall photon dose from “2.7” factor
- Scale the total dose to 0.02 mSv/wk and start again with the first step using the reduced MPD

2 Optimization

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Cost Effectiveness of Laminated Barriers

- Newman and Asadi-Zeydabadi* have used a linear programming technique to optimize the cost of laminated shielding, subject to dose and/or thickness constraints
- They found that steel was a cheaper laminate than lead, contrary to popular construction techniques

* AAPM 2007; SS-FF-T-16

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Optimization: The Cost of Lead

- Until a few weeks ago, the cost of lead was ~\$0.70/lb
- More recently it has climbed to >\$1.75/lb
- Shortage is due to major mine closure in Australia and reduced exports from China

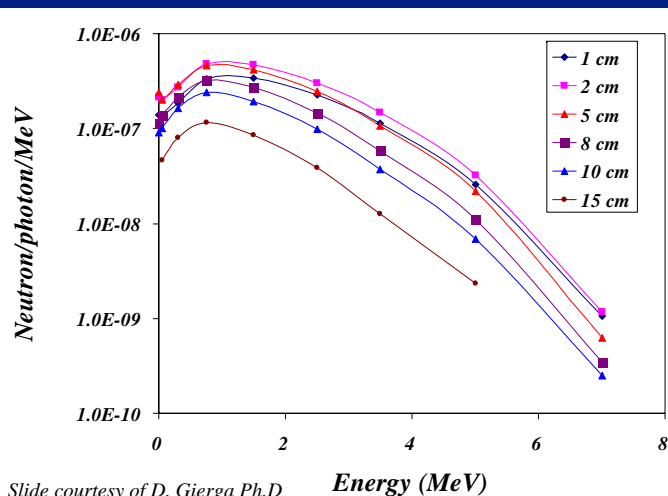
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Thresholds for Photonuclear Reactions

<u>Reaction</u>	<u>Threshold (MeV)</u>
$\gamma + Fe \rightarrow n + \dots$	11.2 (92%)
$\gamma + {}^{206}Pb \rightarrow n + \dots$	8.1
$\gamma + {}^{207}Pb \rightarrow n + \dots$	6.7
$\gamma + {}^{208}Pb \rightarrow n + \dots$	7.4

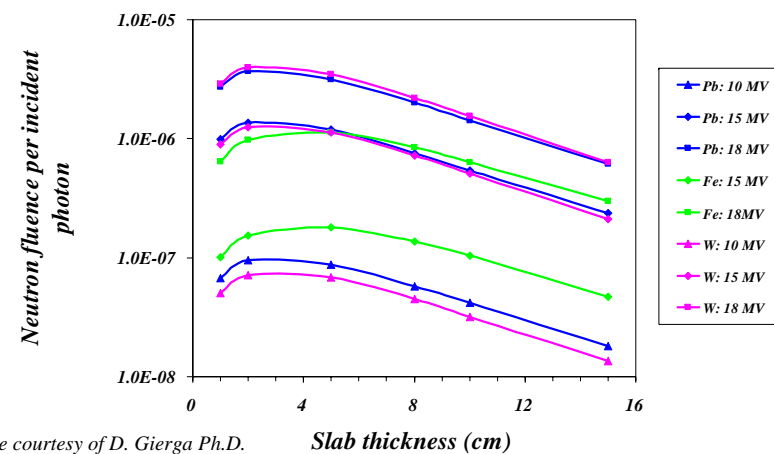
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Neutron Yield vs. Lead Thickness: 18 MV



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Photoneutron Production vs. Thickness



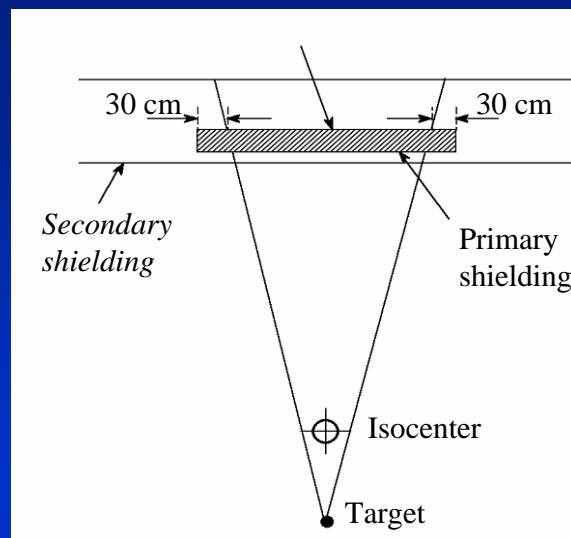
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Photoneutron Ratios

NCRP #151	mSv cGy ⁻¹ m ⁻²	
Pb 18 MV	19	
Fe 18 MV	1.7	
Pb 15 MV	3.5	
Ratios:	NCRP #151	Monte Carlo
	(dose)	(fluence)
18 MV (Pb/Fe)	11.2	4.5
Pb (18 MV/15 MV)	5.4	2.5

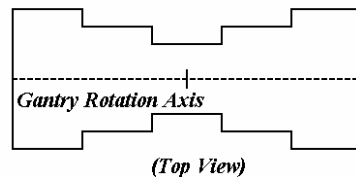
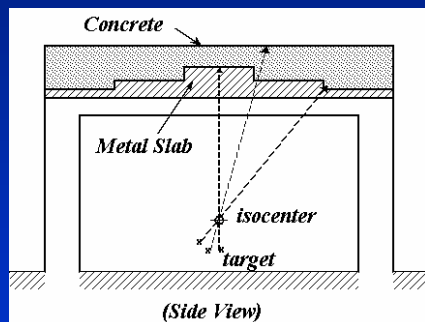
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Width of Primary Barrier



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Contouring the Primary Shielding in the Ceiling



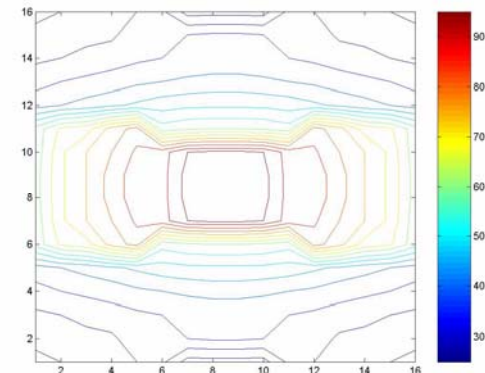
Diagrams courtesy of P. McGinley

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Primary Ceiling Isodose Contours

Programs can help to make the process of determining the isodose curves and, hence the lead “steps”, easier

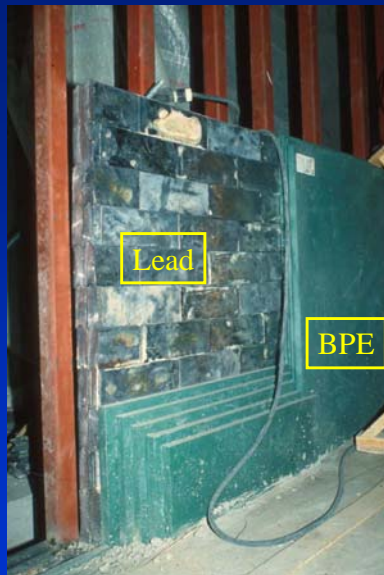
-Biggs.P. Health Physics, 43:601-607, 1982.



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Shielding for 3rd floor IORT machine

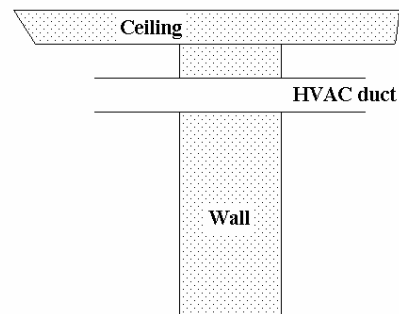
What About Concrete-Free Barriers?



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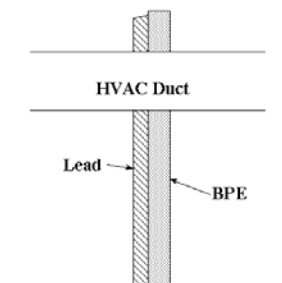
Problem of HVAC Ducts

Standard, Regular Density Construction



Duct width to wall thickness ratio ~0.5

IORT with Pb/BPE Construction

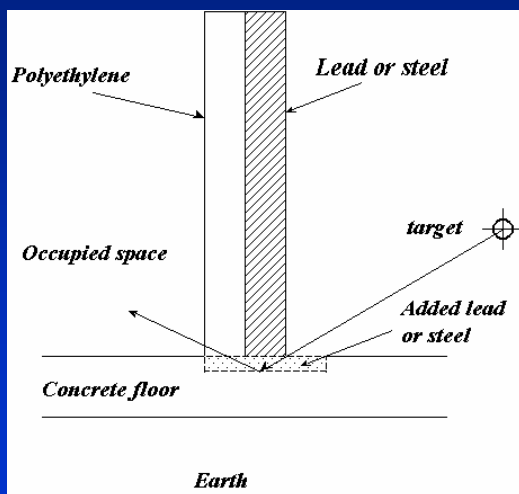


Duct width to wall thickness ratio ~4

(Note that the air handling requirements for an OR are greater than for a treatment room and therefore the duct is much larger)

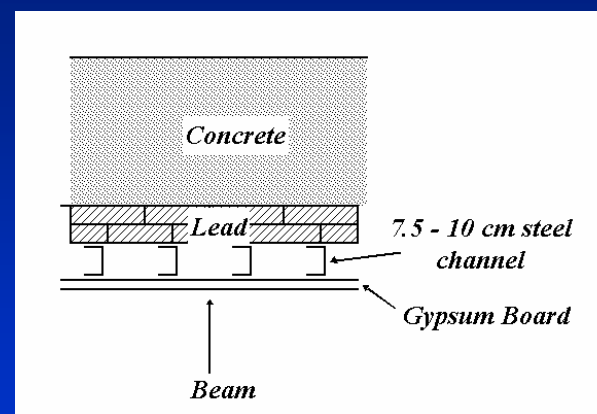
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Lead-Only Room (Photons) : Groundshine

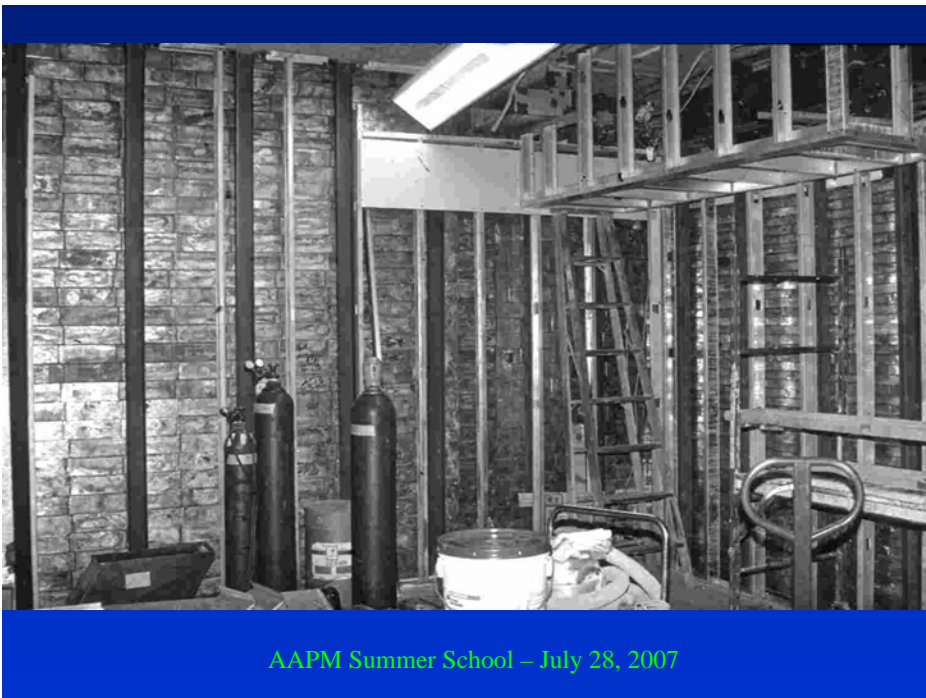


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Upgrading to a High Energy Linac - Wall (1)



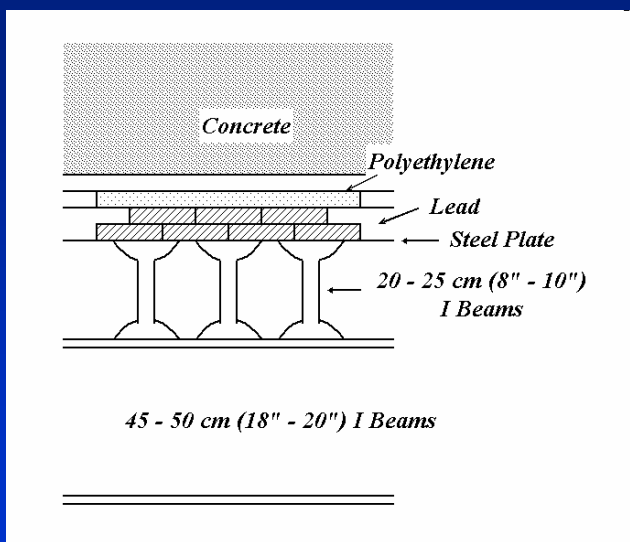
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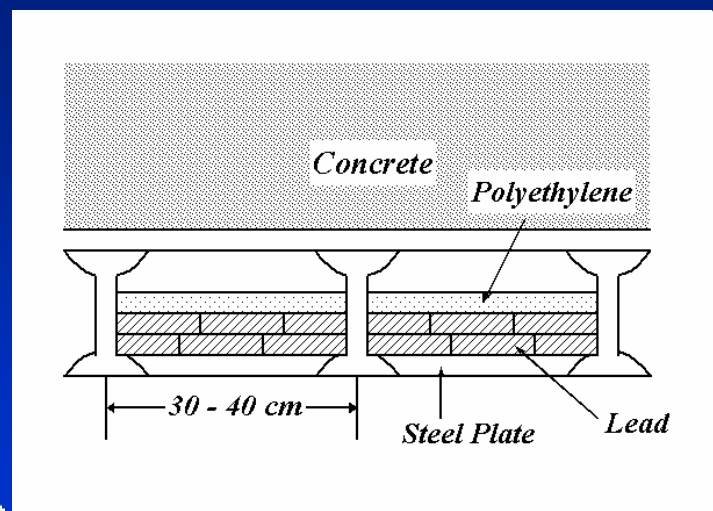


Upgrading to a High Energy Linac - Ceiling (1)



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Upgrading to a High Energy Linac - Ceiling (2)

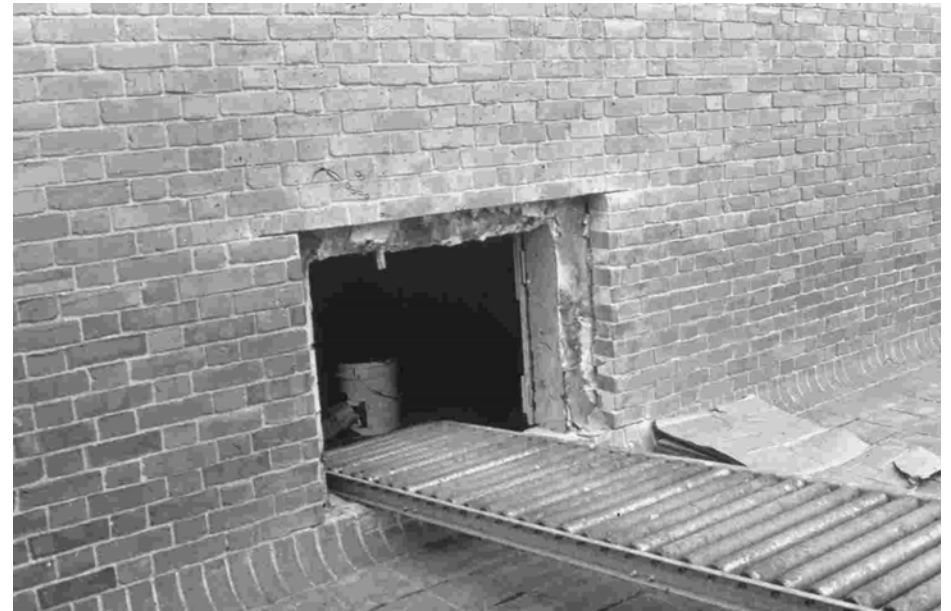


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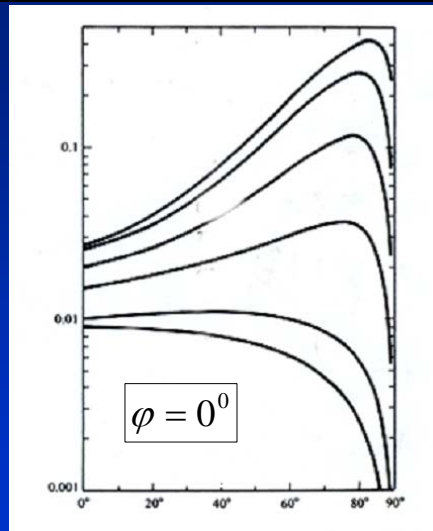
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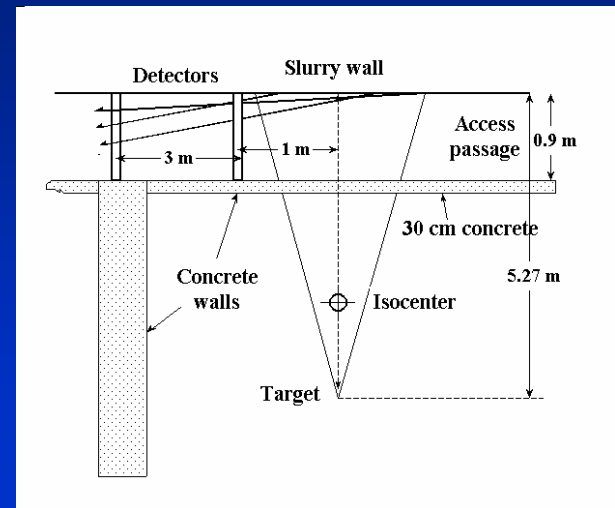
Albedos for In-Plane Scattering

$E_0 = 1.25 \text{ MeV}$
concrete



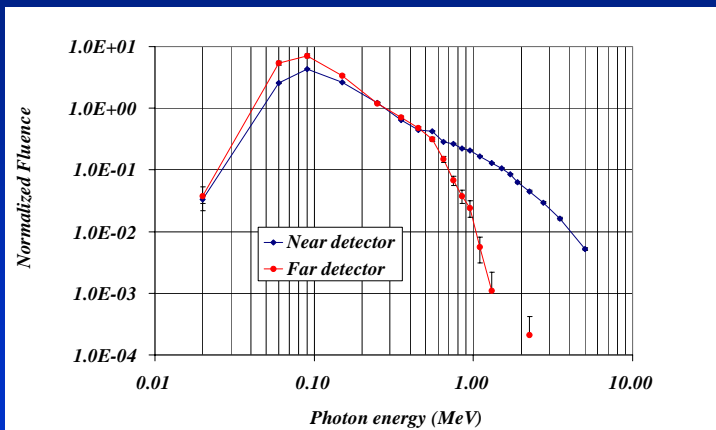
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X-ray spectrum from Primary Scattered at $\sim 90^\circ$



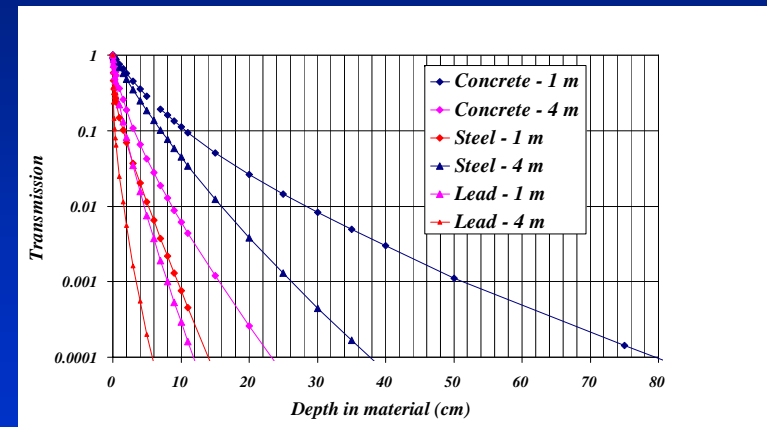
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Spectrum of 90° Scattered Primary Radiation



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Attenuation of 90° Scattered Radiation by Various Materials



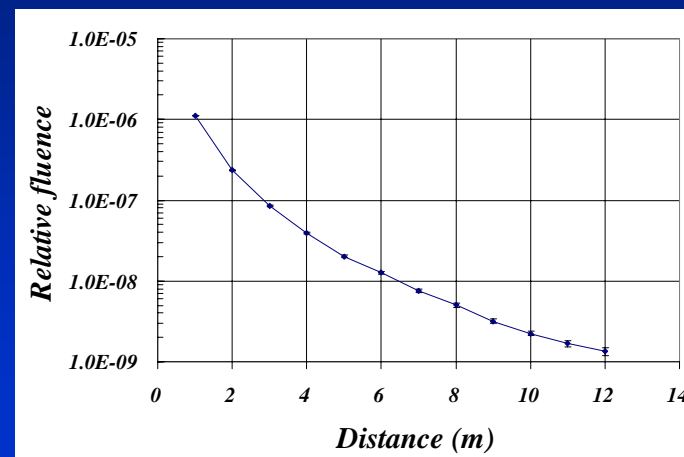
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Material Thickness Required to Reduce Fluence by 10^{-4}

Material Distance (m)	Concrete (cm)	Steel (cm)	Lead (cm)
1	79.3	23.2	14.0
4	37.6	11.8	5.8

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Attenuation of 90° Scattered Primary Radiation



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Doors for High Energy Mazes

- In addition to the scatter and leakage components noted earlier, additional components due to neutrons come into play at high energies (≥ 10 MV)
- These components dominate over the wall-scattered x-ray components
- They consist of neutrons and capture gamma rays from neutron interactions

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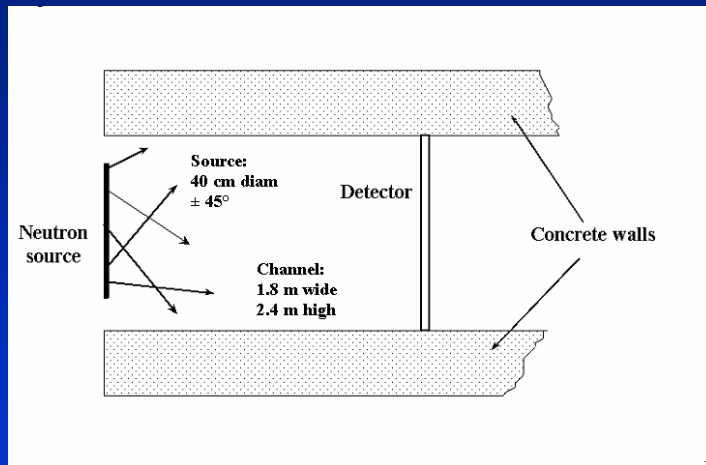
Combined Dose at Maze Door

The neutron and capture γ ray components are calculated and shielding thicknesses to meet the required effective dose equivalent are derived using the following TVLs:

neutrons (100 keV) - 4.5 cm polyethylene
capture γ rays - 6.1 cm lead

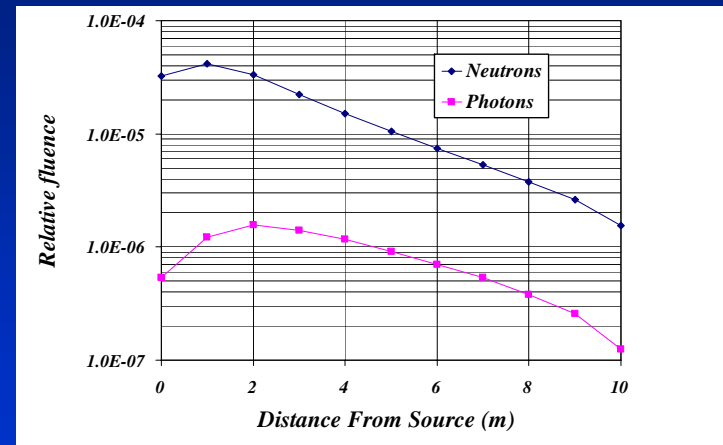
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Neutron production of Capture γ Rays



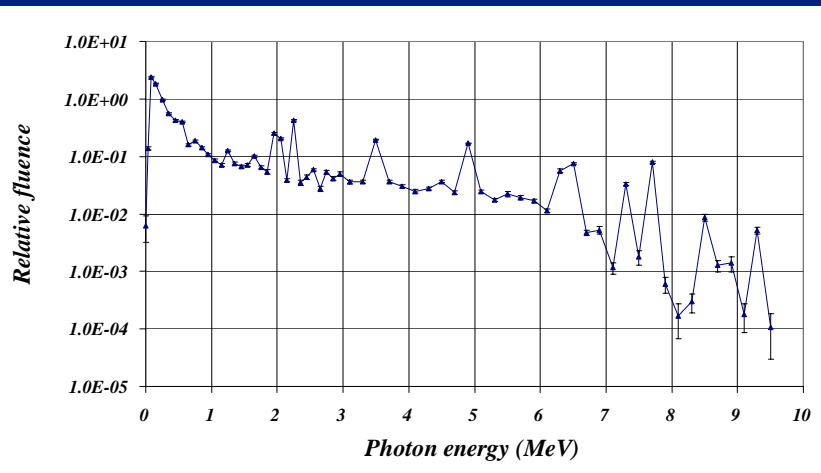
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Photon, Neutron Fluence vs. Distance



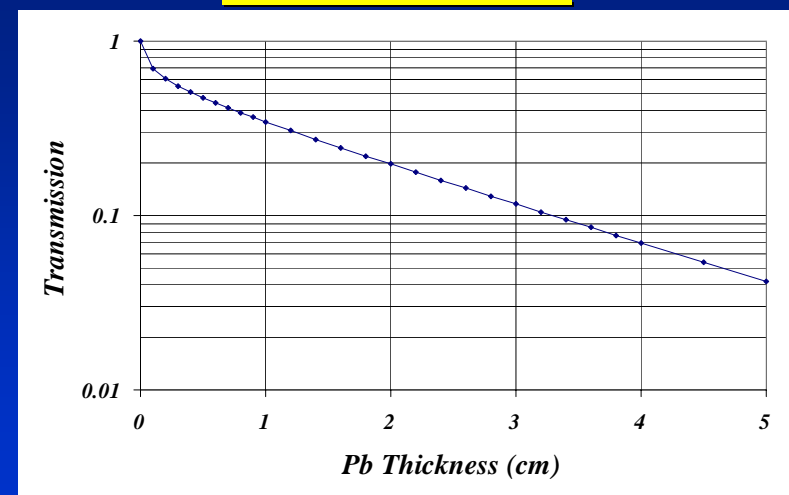
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Capture γ Ray Spectrum



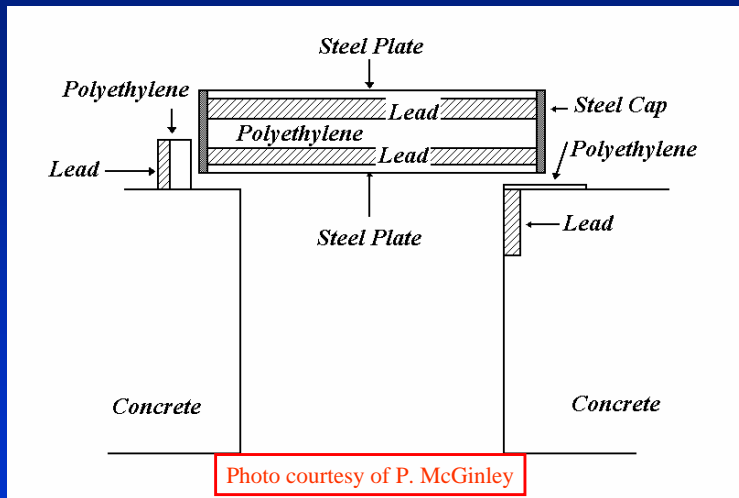
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Attenuation of Neutron-generated Photons in Lead



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High Energy



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Heavy Door Requirements

- All electrical/electronic equipment should be outside the room for ready access
- A come-along should be available to open the door mechanically; this requires a bolt hole in the door and in the wall.

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If the Door Does Not Move: Escape Hatch

- What is its purpose?

If a heavy sliding door fails in the closed position with a patient on the table, there needs to be emergency access. If the problem is not electrical and the come-along does not work, another method of entry is required.

- But is it needed?

The design of current heavy door support systems (overhead rail) minimizes mechanical failure with the door touching the floor. However, ...

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Equipment Needed in Case of Electrical or Mechanical Failure



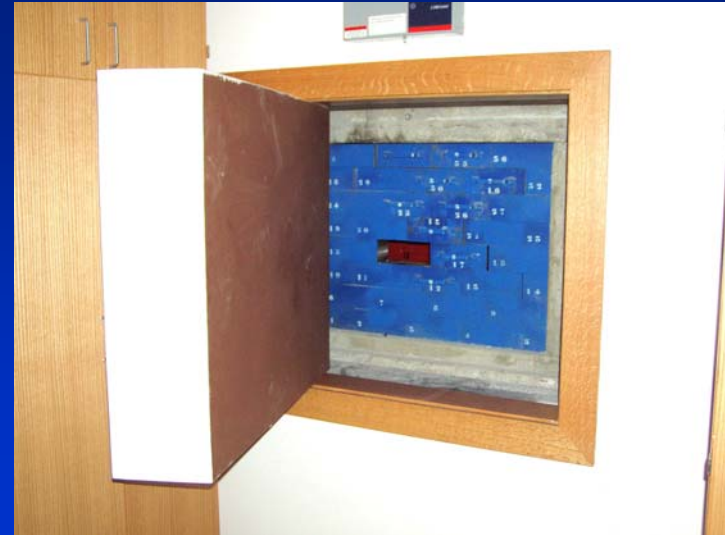
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Escape Hatch Shielding Requirements

- For low energy rooms, lead only, can use two doors, total thickness equivalent to local wall thickness
- For high energy rooms, need lead and polyethylene, total thickness equivalent to local wall thickness for photons and neutrons
- Doors must be linked to the general door interlock chain to ensure that, if opened, the beam will be cut off

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Escape Hatch



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Escape Hatch

Lead/
Polyethylene
combination

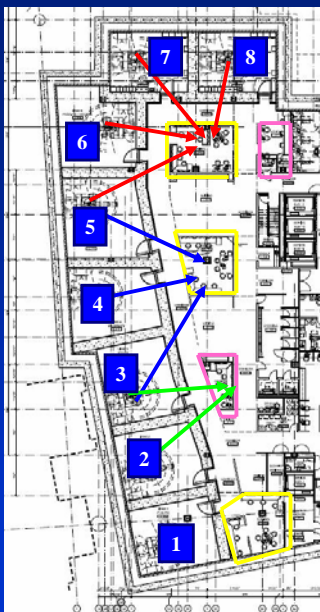


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And now for something completely different ...

- In the talk on Report #147 yesterday, we heard how the issue of “source constraints” was overcome
- We also heard from the PET talks where the need to consider multiple sources was required to compute the dose in various adjacent areas
- In RT, the need sometimes arises to consider the same situation

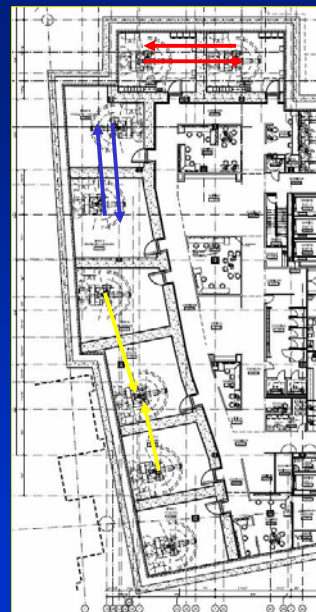
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New Radiation Therapy Department at MGH

Consideration of the impact of multiple sources on maximum permissible doses in RT

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Therapists Receive Dose Inside the Room!

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Summary

- Laminated barriers are commonly used to upgrade old Rx rooms and also in new construction where space is limited
- The methodology for handling laminated barriers is straightforward at low energies, but requires careful consideration of neutrons and capture γ rays for high energies and involves iterative calculations

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Thank you for your attention!



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