

**Quantitative Dosimetry Methods for  
Brachytherapy  
AAPM Summer School  
19 July 2005**

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# What is “Quantitative Dosimetry?”

- **Williamson’s definition: absorbed dose estimation method providing**
  - Accurate representation of well-defined physical quality
  - Rigorous uncertainty analysis  $\Rightarrow$   $<10\%$  uncertainty 0.5 to 5 cm in liquid water
  - Traceable to NIST primary standards ( $S_{K,N99}$ )
- **Applications**
  - Single-source dose-rate arrays for TG-43 parameter determination (“Reference quality” dose distributions)
  - Direct treatment planning
  - Validating semi-empirical algorithms

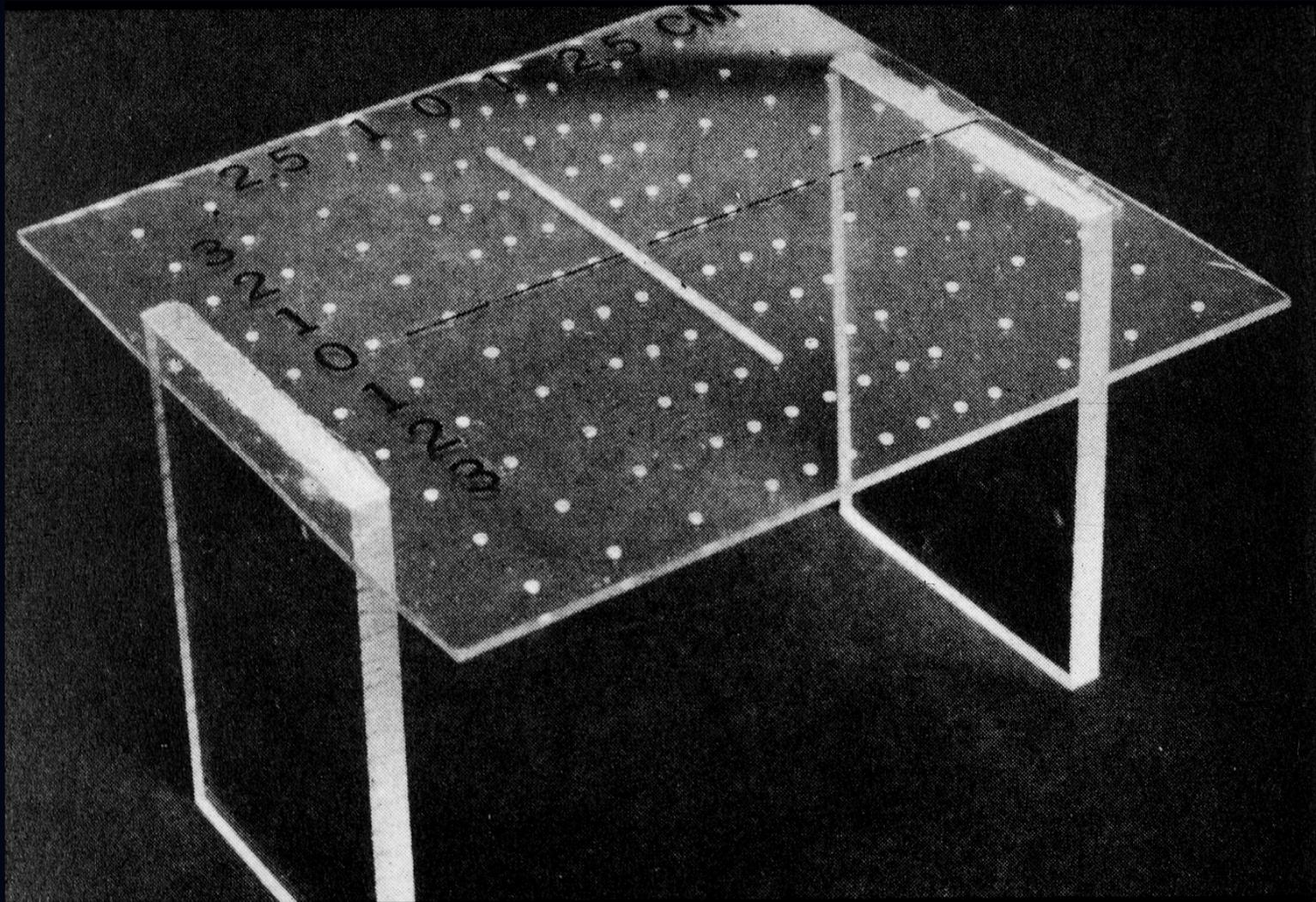
# Outline

- **Experimental Techniques**
  - TLD dosimetry: current standard of practice
  - Emerging experimental techniques
- **Monte Carlo-based dosimetry**
- **Results of TLD and MC dosimetry**
  - Uncertainty analysis
  - Agreement

## Quantitative Dosimetry Era: 1980-

- 1955 Tochlin: Film Dosimetry
- 1966 Lin & Kenny: TLD dosimetry in medium
- 1983 Ling: Diode dosimetry of I-125 seeds
- 1985 Loftus: I-125 exposure standard
- 1986 NIH ICWG contract
  - Nath, Anderson, Weaver: Validation of TLD dosimetry
- 1983 Williamson: Monte Carlo dosimetry
- 1994 Task Group 43 Report

**TLD dose measurements around  $^{226}\text{Ra}$  Needle  
Lin and Cameron: Univ. of Wisconsin, 1965**



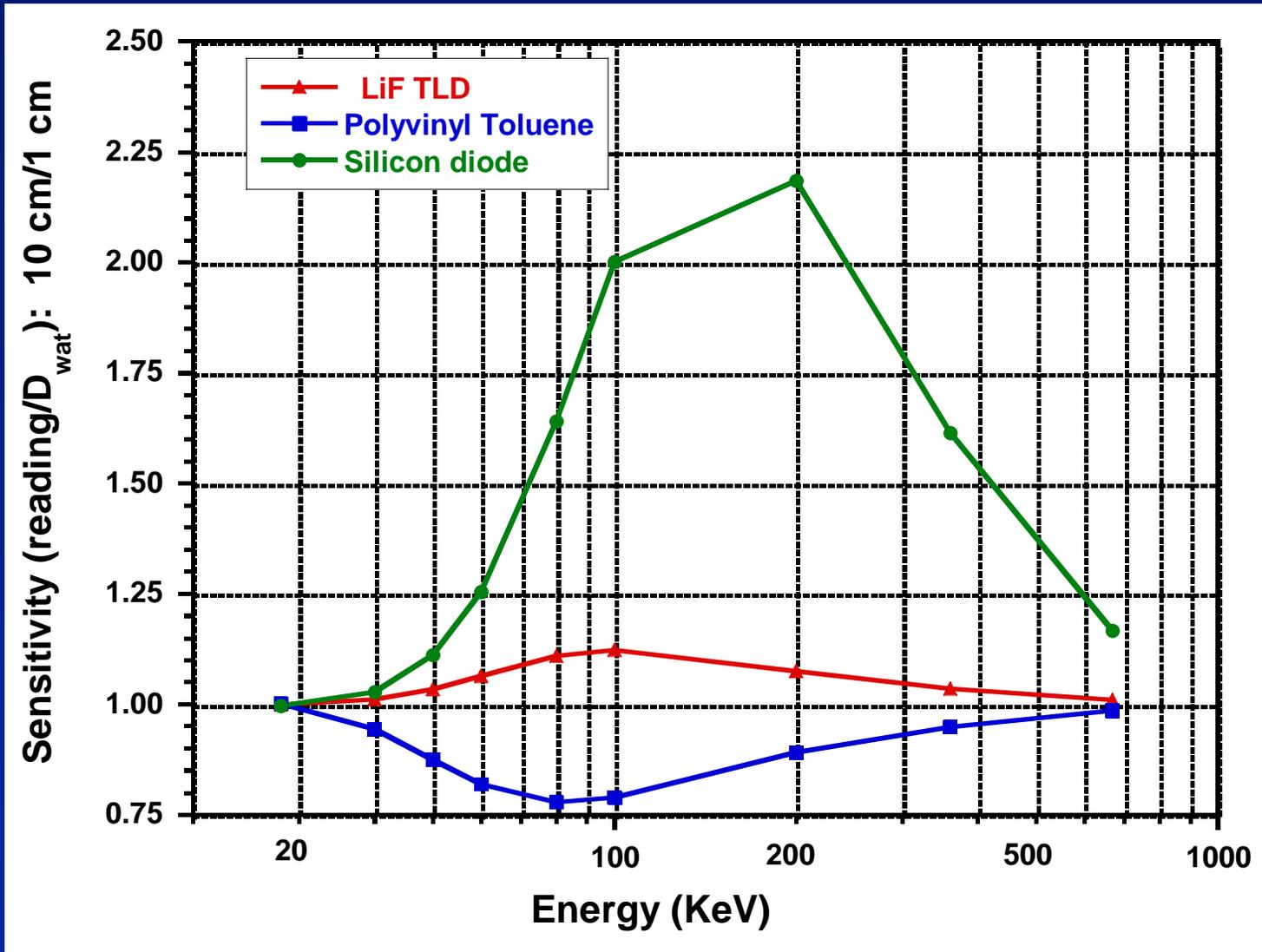
# Dosimetric Environment

- **Large Dose Gradients**
  - Wide Range of Dose Rates
  - Positioning accuracy needed for 2 % dose accuracy
    - 2 mm Distance      $\pm 20 \mu\text{m}$
    - 5 mm Distance      $\pm 50 \mu\text{m}$
    - 10 mm Distance    $\pm 100 \mu\text{m}$
  - Large Number of Measurements Needed
- **Low Photon Energies**
- **Relatively Low Dose Rates**

# Criteria for experimental dosimeters

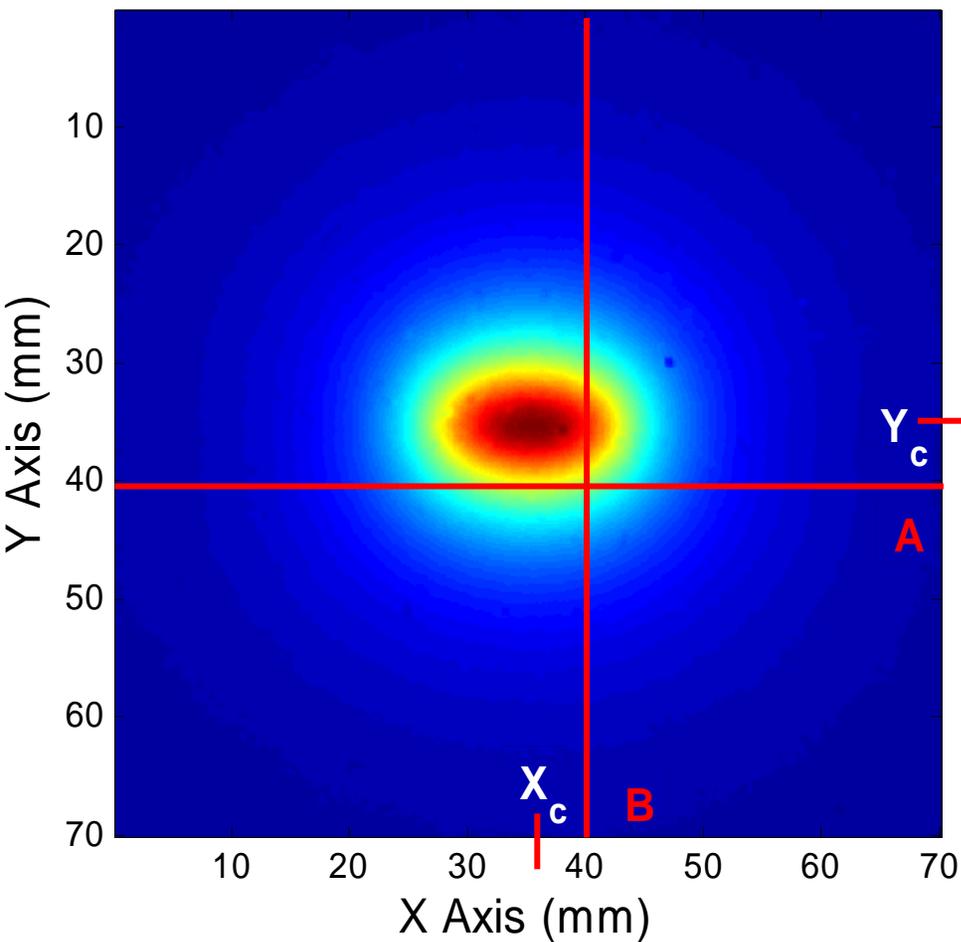
- **Signal stability and reproducibility**
  - Spatially and temporally constant **Sensitivity** (signal/dose)
  - Free of fading, dose-rate effects
  - Good signal-to-noise ratio (SNR)
- **Small size, high sensitivity, large dynamic range**
  - Small size: avoid averaging dose gradients
  - Large size: Good signal at low doses
- **Good positioning accuracy**
- **Support measurements at many points**

# Sensitivity (10 cm)/Sensitivity (1 cm) vs energy

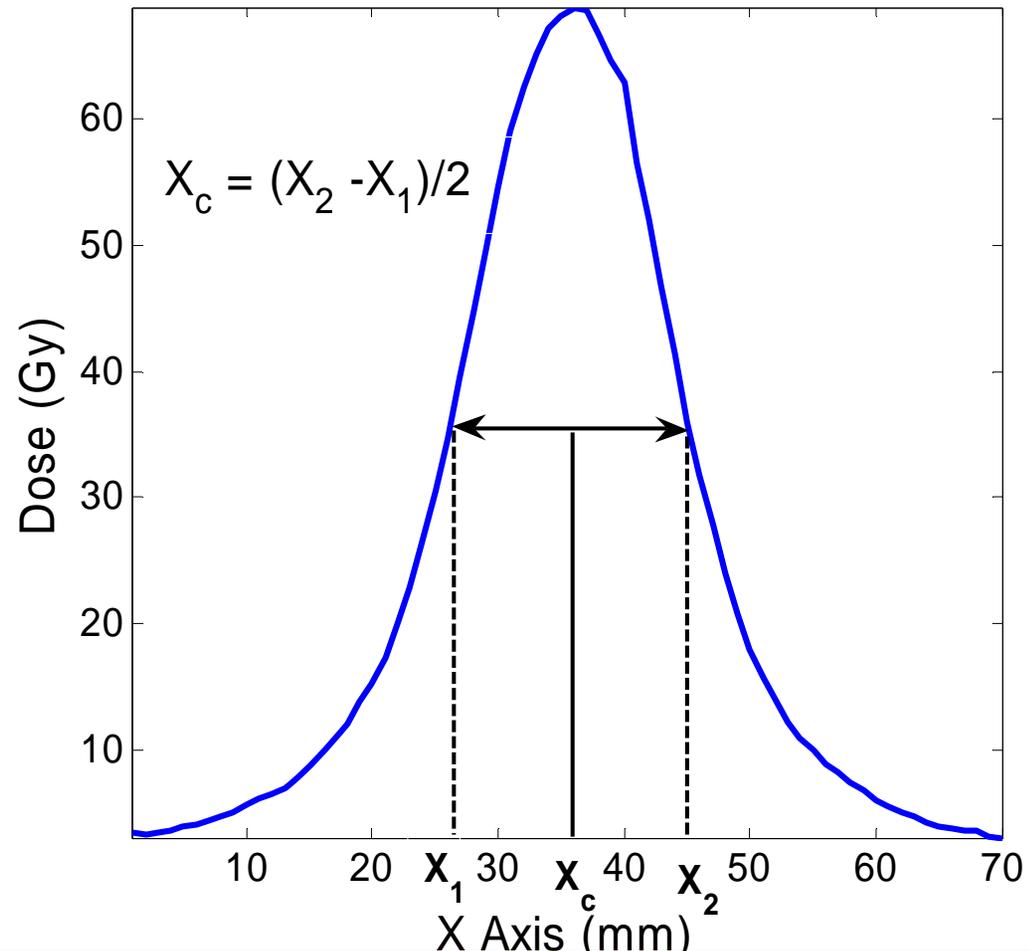


# Localization via Digital Dosimeters

2D dose distribution



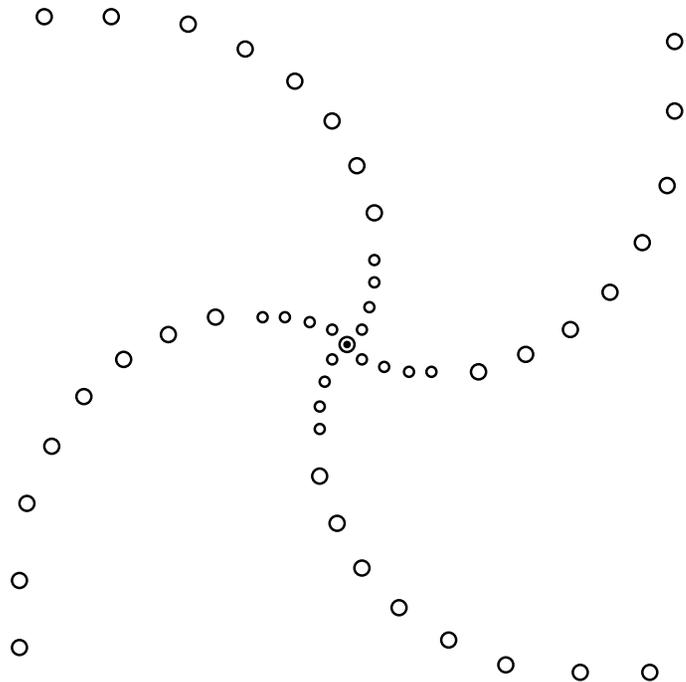
Profile A



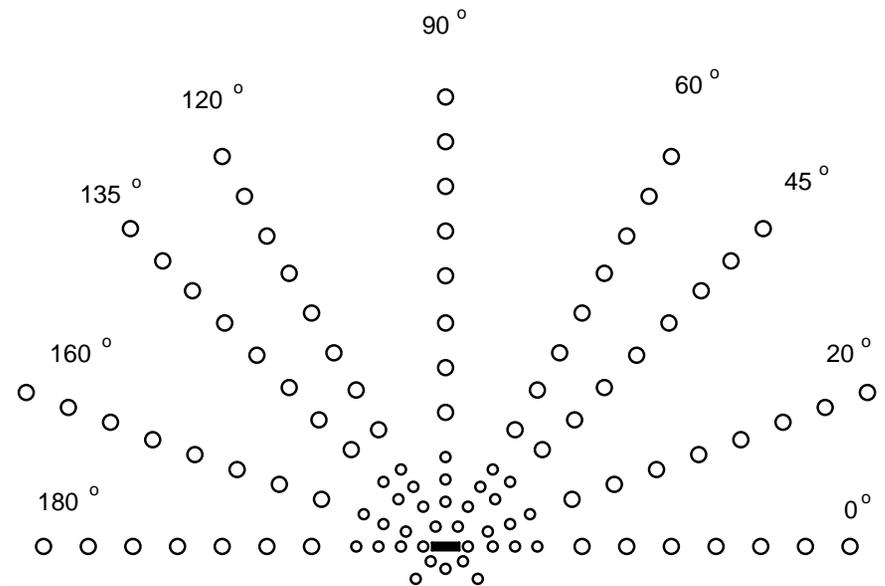
**30-100  $\mu\text{m}$  positional accuracy achievable**

# Solid Water Phantoms for TLD Dosimetry

Transverse Axis Measurement Phantom



Polar Dose Profile Measurement Phantom

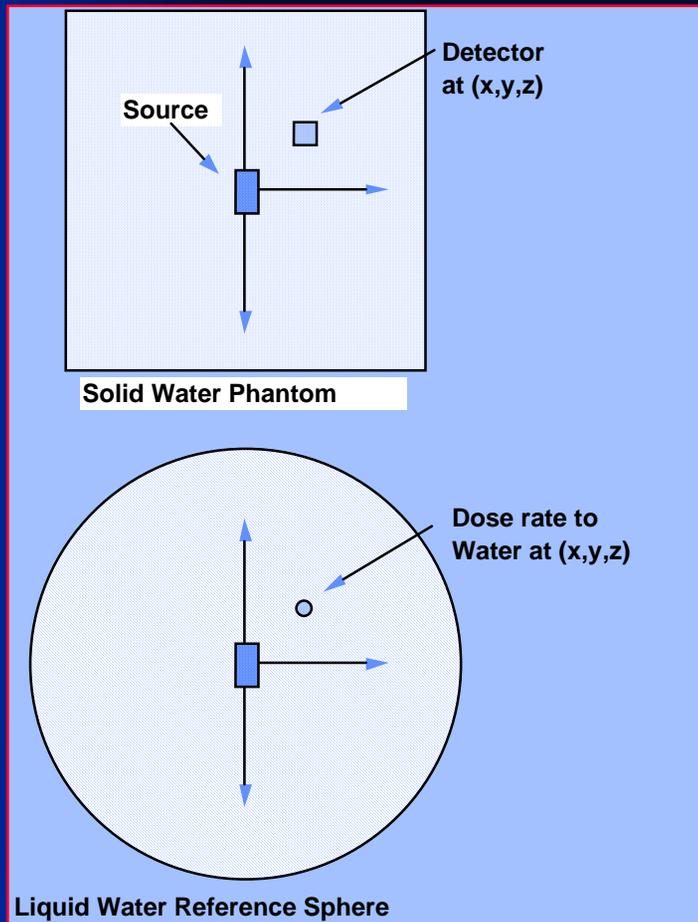


**100-200  $\mu\text{m}$  positional accuracy achievable**

# TLD Detectors

- Use TLD-100 LiF extruded ribbons ('chips')
  - 1 x 1 x 1 mm<sup>3</sup> at distances < 2 cm
  - 3 x 3 x 0.9 mm<sup>3</sup> at distances ≥ 2 cm
- Use RMI 453 Machined Solid Water Phantom
  - Composition (CaCO<sub>3</sub> + organic foam) not stable
  - Either perform chemical assay or use high purity PMMA
- Annealing protocol
  - 1 hour 400° C followed by 24 hours of 80° C pre-irradiation
  - OR
  - 1 hour 400° C pre-irradiation followed by 10 minutes at 100° C Post-irradiation

# Brachytherapy Dosimetry



- **Given:**  $R_{\text{det}}(\vec{r})$  Relative solid state dosimeter reading (TLD or Diode)
- **Desired:**  $D_{\text{wat}}(\vec{r})$  absorbed dose to water
- **Corrected for:**
  - Detector sensitivity
  - Measurement vs reference geometry
  - Radiation field Perturbation
  - Detector response artifacts

# Brachytherapy Dose Measurement

$$\left[ \frac{\dot{D}_{\text{wat}}(\vec{r})}{S_K} \right]_{\text{meas}}^{\text{BRx}} = \frac{R_{\text{det}}(\vec{r}) \cdot g(T)}{S_K \cdot \varepsilon_{\lambda} \cdot E(\vec{r})}$$

$$\varepsilon_{\lambda} = \left[ R_{\text{det}} / D_{\text{med}} \right]_{\text{meas}}^{\lambda}$$

is measured Response in calibration beam,  $\lambda$

$$E(\vec{r}) = \frac{\left[ R_{\text{det}} / D_{\text{wat}} \right]_{\text{BRx}} \text{ at } \vec{r}}{\varepsilon_{\lambda}}$$

is relative detector response at  $\vec{r}$  in Brachytherapy geometry

- $S_K$  = Measured Air-Kerma Strength
- $g(T)$  = 1/effective exposure time (decay correction)

## TLD readings

$$\langle R_{\text{TLD}}(\vec{r}) \rangle = \frac{1}{n} \sum_{i=1}^n \frac{(\text{TL}_i - \text{TL}_{\text{bkgd}})}{F_{\text{lin}} \cdot S_i}$$

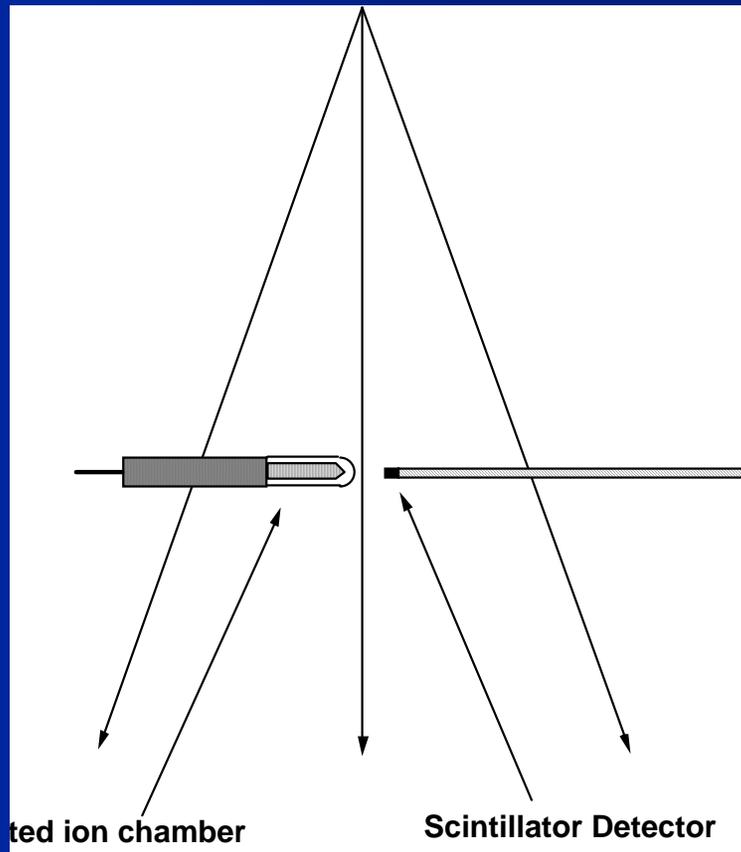
- $\text{TL}_i$  is Measured Response of  $i$ -th detector at  $r$
- $F_{\text{lin}}(\text{TL})$  is non-linearity correction for net response TL
- $S_i$  is relative sensitivity of  $i$ -th detector derived from reading TLDs exposed to uniform doses
- TG-43 recommends  $n = 5-15$

# Relative Energy Response

$$\begin{aligned} E(\vec{r}) &= \frac{[\langle \text{TL}(\vec{r}) \rangle / D_{\text{wat}}(\vec{r})]}{[\langle \text{TL} \rangle / D_{\text{med}}]} \text{ for Brachy Source} \\ &= \frac{\varepsilon_{\text{BRx}}(\text{TL}_0, \vec{r})}{\varepsilon_{\lambda}(\text{TL}_0)} \text{ for same TL}_0 \end{aligned}$$

- **E(d) obtained by**
  - Measuring TLD response in free air as function of average energy in low energy x-ray beams
  - Monte Carlo calculations
  - Analytic calculations
- **Generally assumed to be independent of position**

# Compare detector to “matched” X-ray Beam calibration in Free-Air $h\nu = 40-120$ kVp



TL = TLD mean net reading

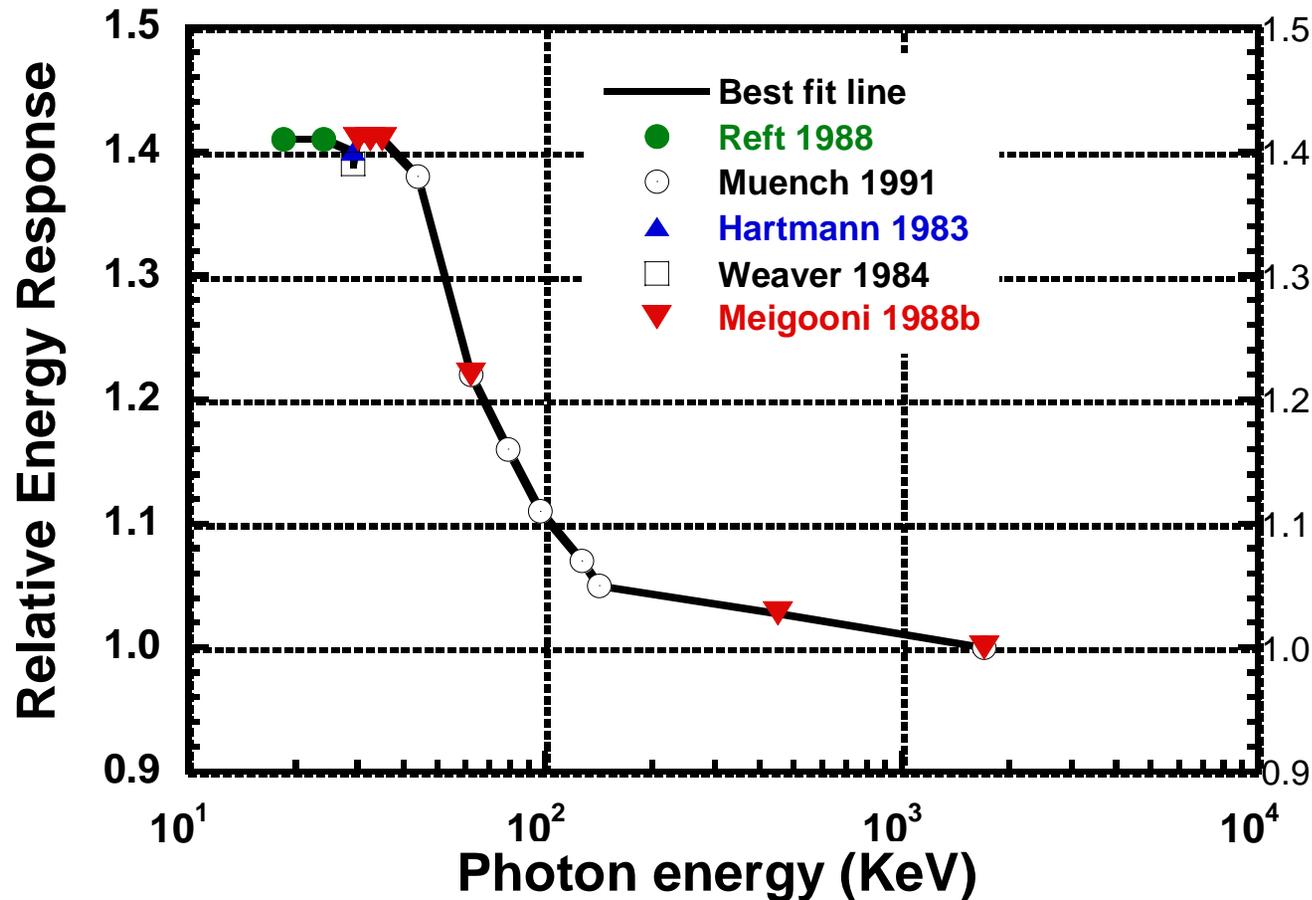
$K_{\text{air}}^{\text{FS}}$  = measured air kerma

$$E(\mathbf{r}) = \left( \frac{\text{TL}}{K_{\text{air}}^{\text{FS}}} \right)_{\text{Meas}}^{h\nu} \cdot \frac{(K_{\text{air}} / D_{\text{wat}})_{\text{MC}}^{h\nu}}{c_{\text{repl}} \cdot c_{\text{disp}}(\mathbf{r}) \cdot \epsilon_{\lambda}}$$

$$c_{\text{repl}} = \frac{D_{\text{wat}} \text{ in medium}}{K_{\text{wat}}^{\text{FS}} \text{ in cavity}} \approx 0.97$$

$$c_{\text{disp}}(\mathbf{r}) = D_{\text{wat}}(\vec{\mathbf{r}}) \text{ at point} / \left[ \frac{1}{V(\vec{\mathbf{r}})} \int_{V(\vec{\mathbf{r}})} D_{\text{wat}}(\vec{\mathbf{r}}') dV' \right] \in (0.80 - 1.00)$$

# Measured E factors



- Conventional choice:  $E=1.4$  w/o regard to details
- Hence, 2004 TG-43 has assigned 5% uncertainty to  $E$

# Monte Carlo Evaluation of E(d)

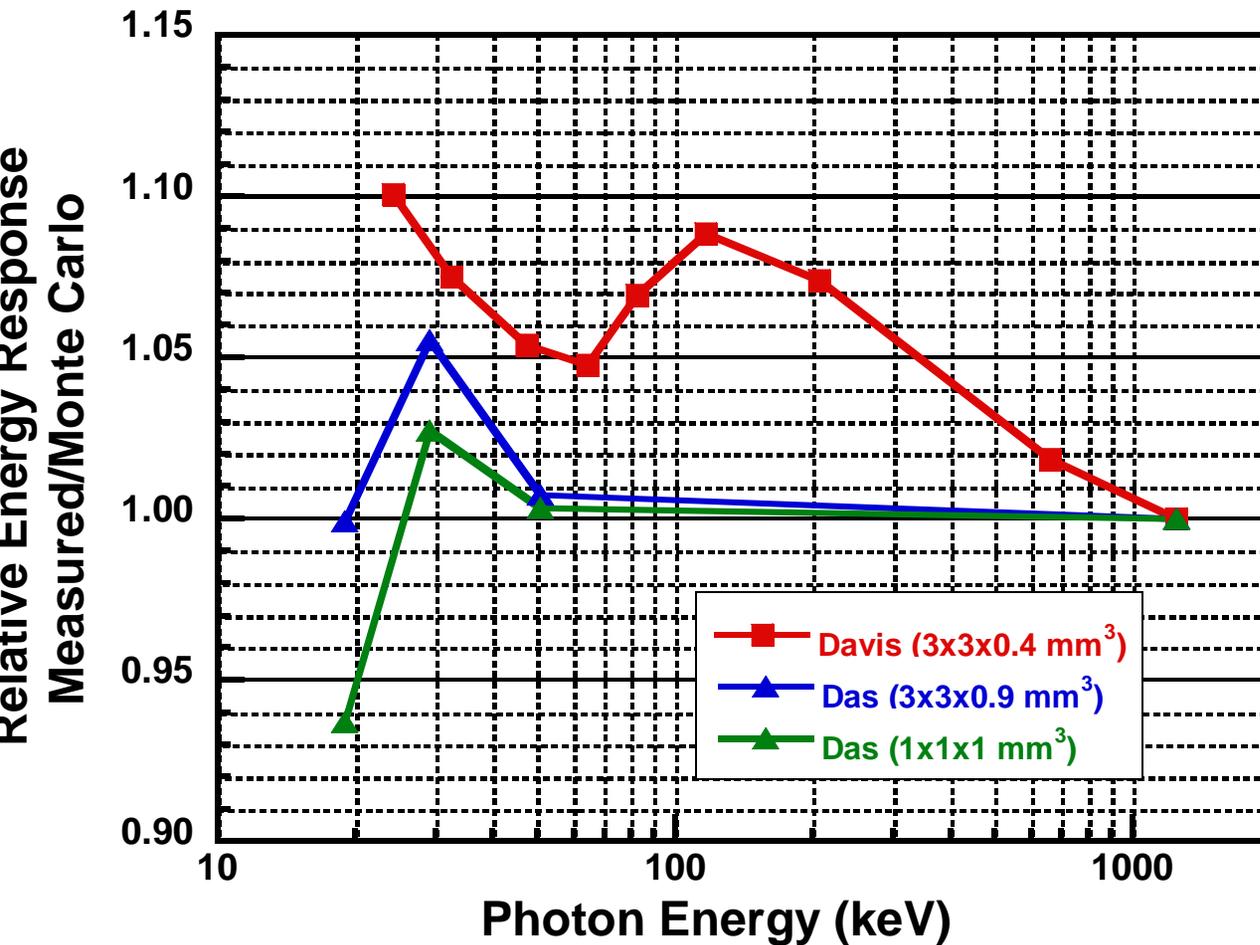
- **E(d) Corrects for**
  - Measurement medium and geometry vs water
  - Calibration medium vs. water
  - Detector artifacts: Energy response, volume averaging, angular anisotropy, self attenuation
- **Assume: Detector response  $\star$  energy imparted to active volume for beam qualities  $\lambda$**

If 
$$\mathbf{R}_{\text{det}}^{\lambda} = \alpha \cdot \mathbf{D}_{\text{det}}^{\lambda}$$

Then 
$$\mathbf{E}(\vec{\mathbf{r}}) = \frac{[\Delta \mathbf{D}_{\text{det}}(\vec{\mathbf{r}}) / \Delta \mathbf{D}_{\text{wat}}(\vec{\mathbf{r}})]_{\text{BRx}}^{\text{MC}}}{[\Delta \mathbf{D}_{\text{det}} / \Delta \mathbf{D}_{\text{med}}]_{\lambda}^{\text{MC}}}$$

# Measured vs. Calculated E(d)

Davis 2003 and Das 1995



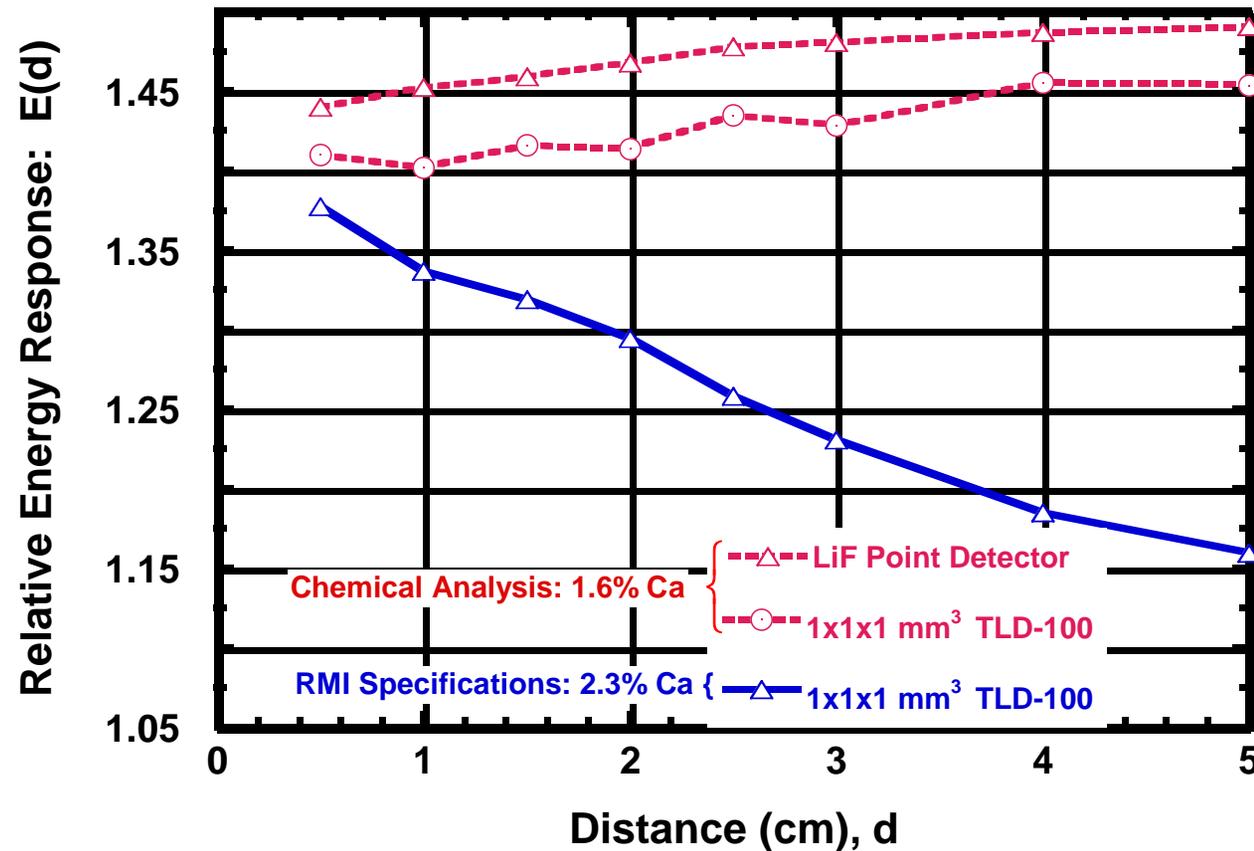
$R_\lambda = \text{TL at energy } \lambda$

$K_{\text{air}}^\lambda = \text{measured air kerma}$

$$\alpha_\lambda = \frac{(\text{TL}/K_{\text{air}})_{\text{Meas}}^\lambda}{(\text{D}_{\text{TLD}}/K_{\text{air}})_{\text{MC}}^\lambda}$$

Energy linearity of TLD is controversial

# I-125 Seed E(d) in Solid Water



- Solid-to-Liquid Water correction: 4%-15% at 1-5 cm
- 10-30% variations in SW composition reported: 5%-20% dosimetric errors

## **Summary: TLD phantom dosimetry**

- **1-3 mm size  $\Rightarrow$  precision: 2-5% above 1 cGy**
- **Energy response corrections**
  - Distance independent, excluding phantom corrections
  - Energy linearity is controversial (<10%)
  - Many corrections routinely ignored
- **Widely-used SW phantom has uncertain composition**
  - High-purity industrial plastics recommended
- **Extensive benchmarking of TLD vs Monte Carlo**
  - 3-10% agreement for Pd-103 and I-125 sources
  - 7%-10% absolute dose measurement uncertainty

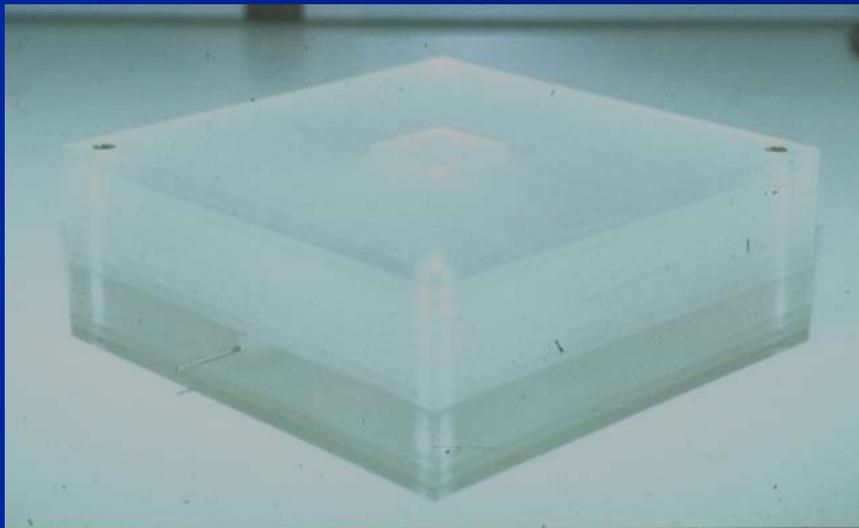
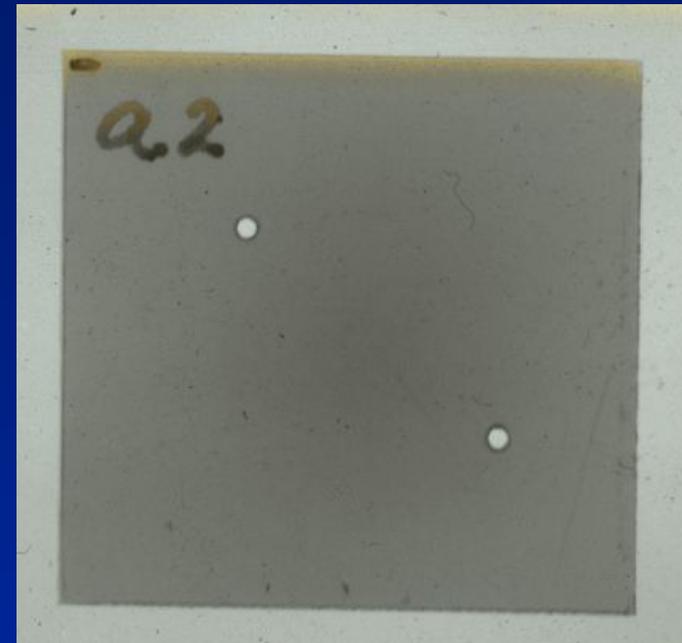
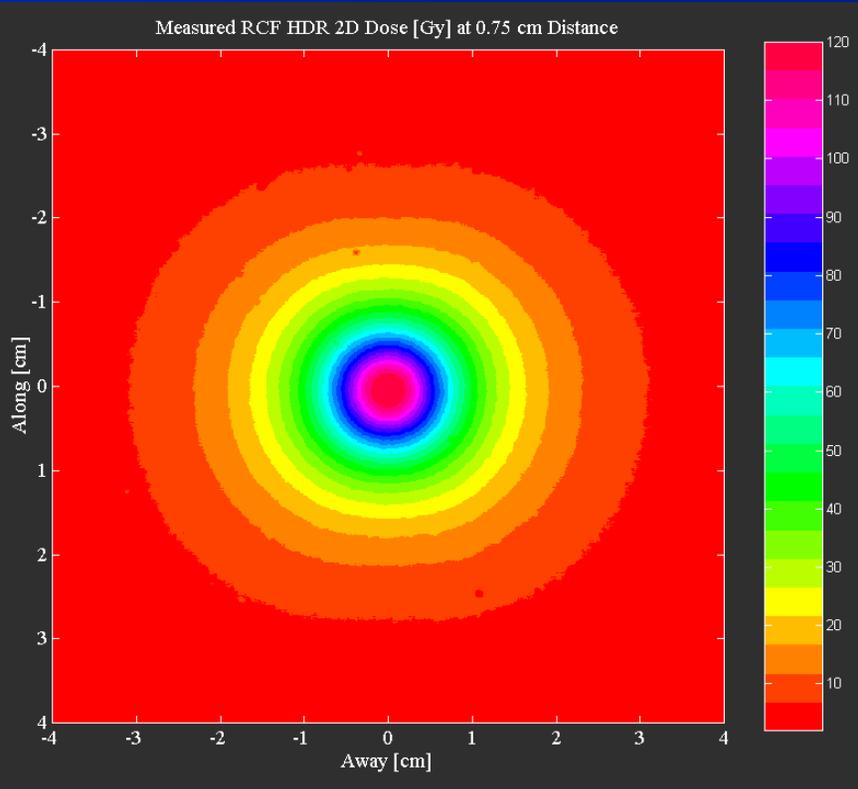
## Other dosimetry systems

- **Plastic scintillator (PS) and diode probes**
  - High sensitivity, small size, good SNR, and waterproof
  - Single element detectors requiring water scanning system
- **PS: established as transfer/relative dosimeter for beta sources**
  - » Large (30%) energy nonlinearity
- **Diode: underutilized in presenter's opinion**
  - Energy linearity well established
  - Large  $E(d)$  variation for medium energy sources
  - Well established as relative dosimeter

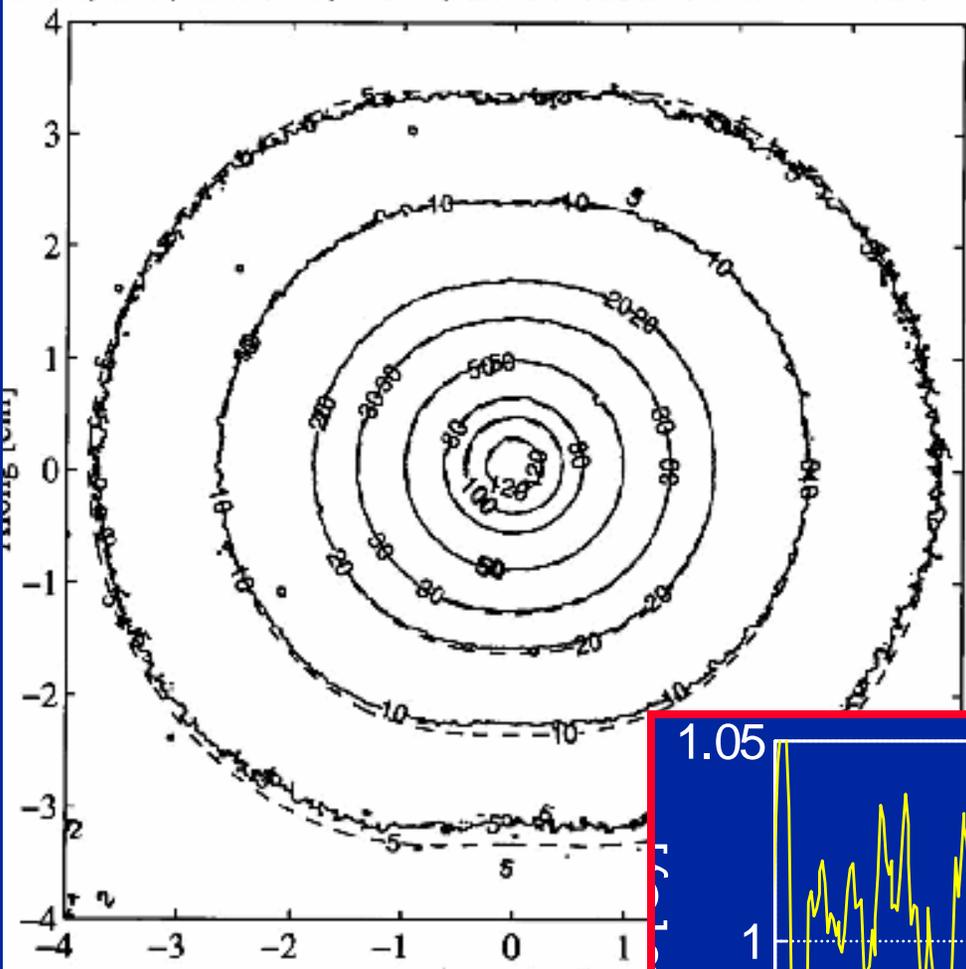
# Emerging Dosimetry Systems

## 2D RadioChromic Film

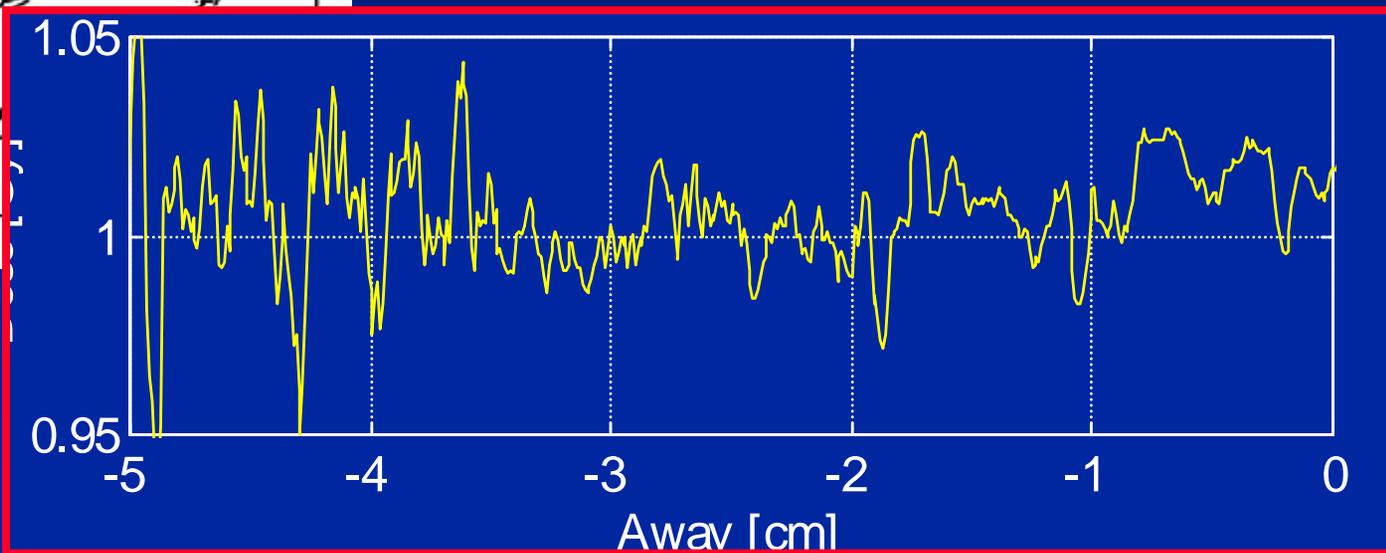
### Ir-192 HDR Source



RCF(Solid) & MCPT(Dashed) HDR Isodose Curves 0.75 cm Distance

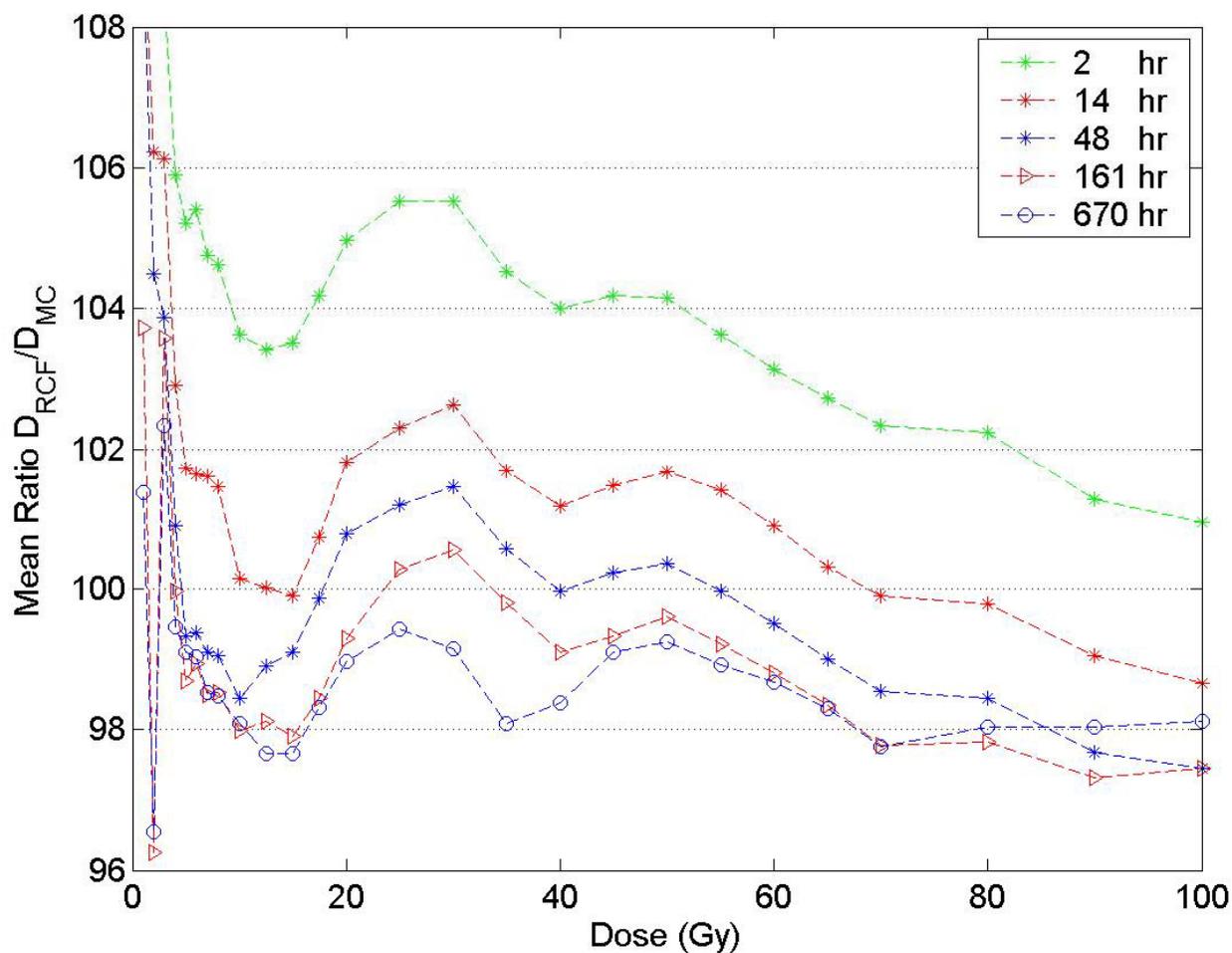


**Absolute RCF Dose  
Measurement vs  
Monte Carlo  
HDR  $^{192}\text{Ir}$  Source  
RCF  $2\sigma$  uncertainty: 4.6%**



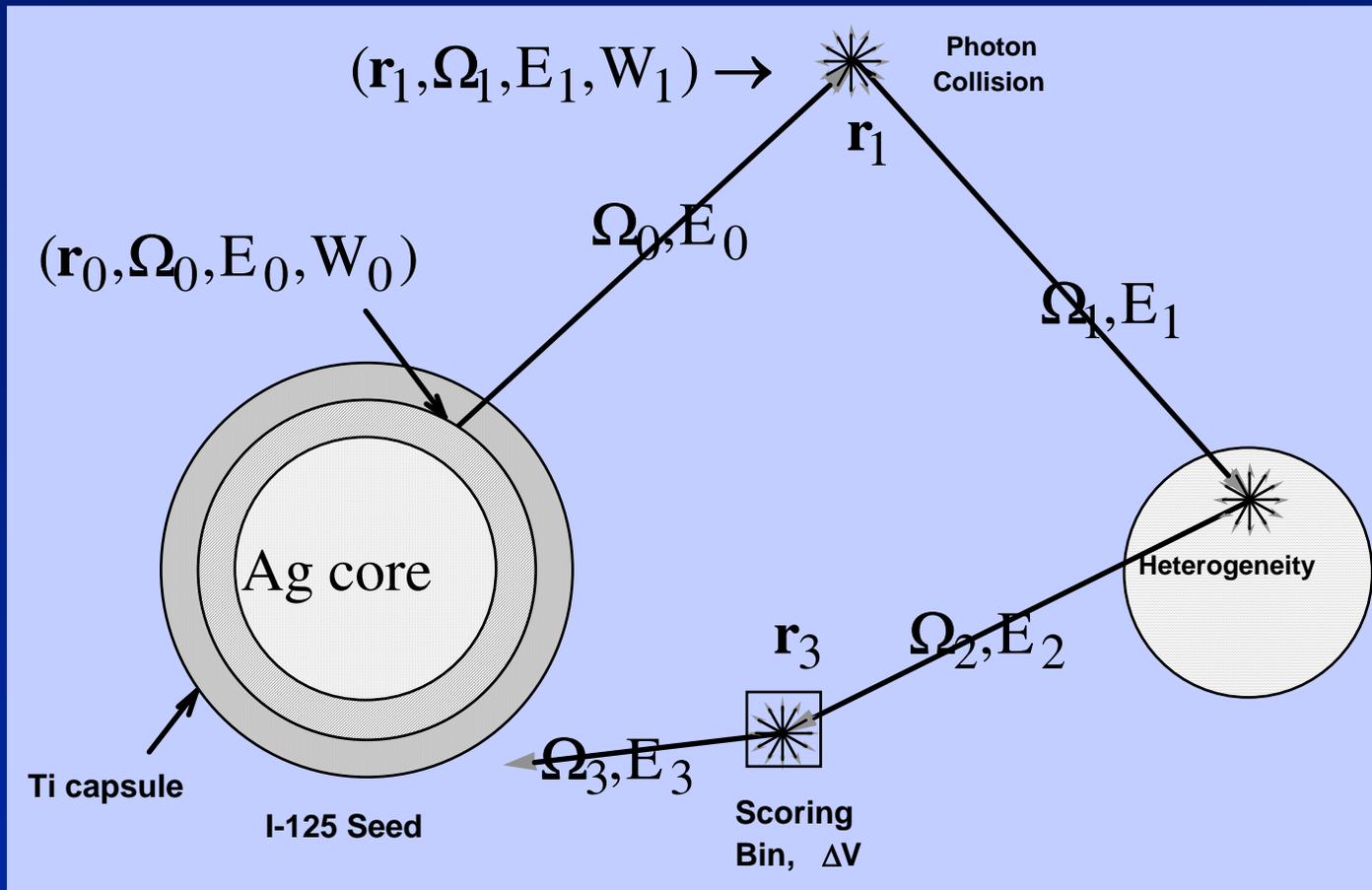
# Absolute RCF dosimetry for LDR Sources

## Cs-137: RCF/MC vs. Exposure-to-densitometry time interval



- Mean error vs dose
- 6 day exposure
- Very high 100  $\mu\text{m}$  spatial resolution
- Fading artifacts not significant
- Energy linearity within 5%

# Monte Carlo Simulation Typical Trajectory



# **Monte Carlo Technical Issues**

## **Particle Collision Dynamics**

**Total and differential cross sections for all collision processes and media**

## **Geometric Model**

**Size, location, shape, composition and topology of each material object**

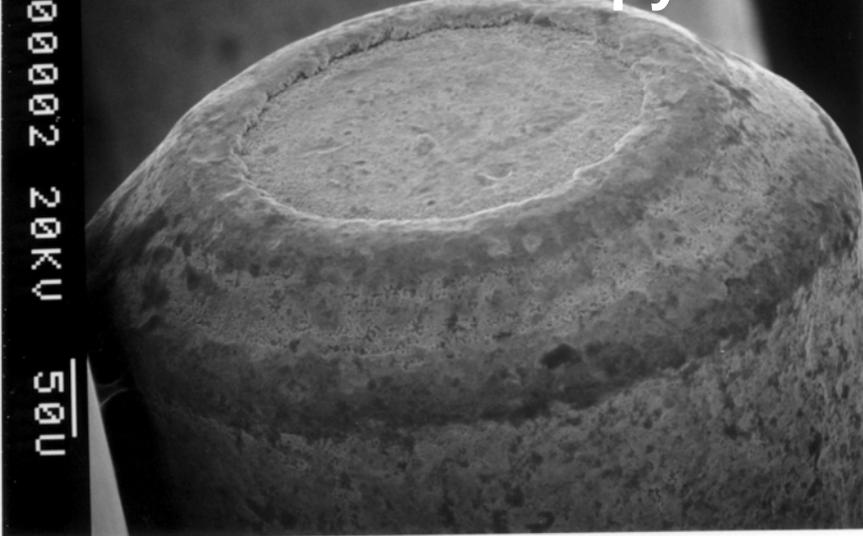
## **Detector Model**

**relationship between dose and collision density**

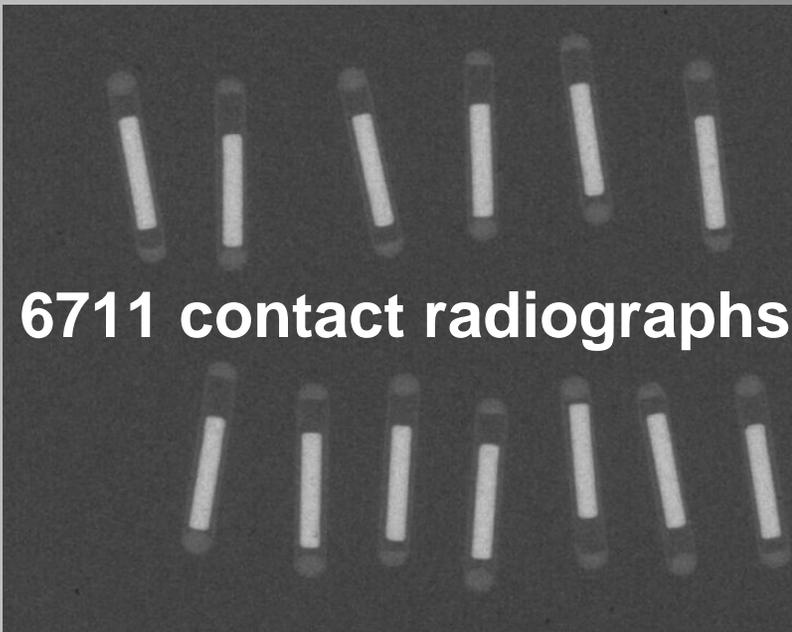
# Collisional Physics Requirements for Low-Energy Brachytherapy

- **Only photon transport needed**
  - Secondary CPE obtains (Dose  $\approx$  Kerma)
  - Neutral-particle variance reduction techniques useful
- **Comprehensive model of photon collisions**
  - **NIST EXCOM or EPDL97 Cross sections are essential!!**
  - Coherent scattering and electron binding corrections
    - » Use molecular/condensed medium form factors
  - Characteristic x-ray emission from photo effect
  - Approximations OK for some RTP applications
- **Options: MCNP, EGSnrc and VCU's PTRAN\_CCG**

6711 silver rod end  
Electron microscopy

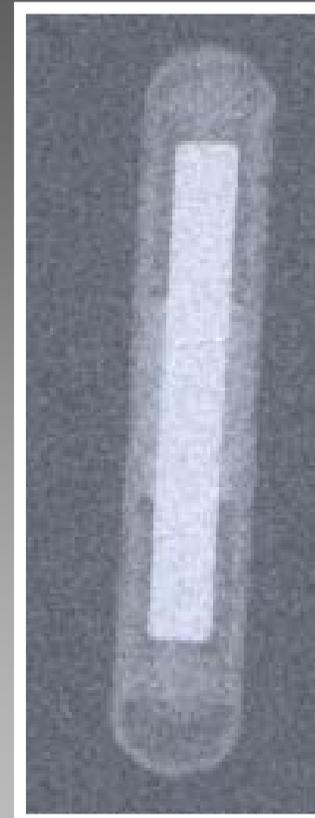


6711 contact radiographs

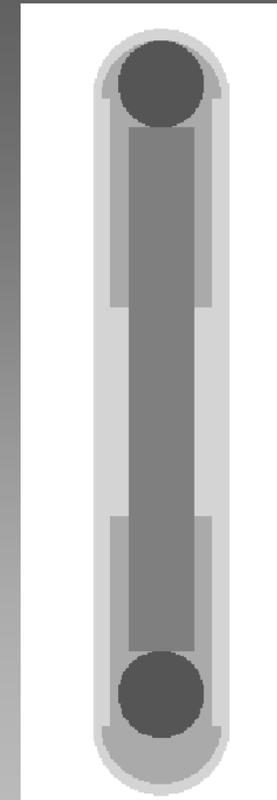


# Geometric Model Validation

DraxImage I-125 Seed



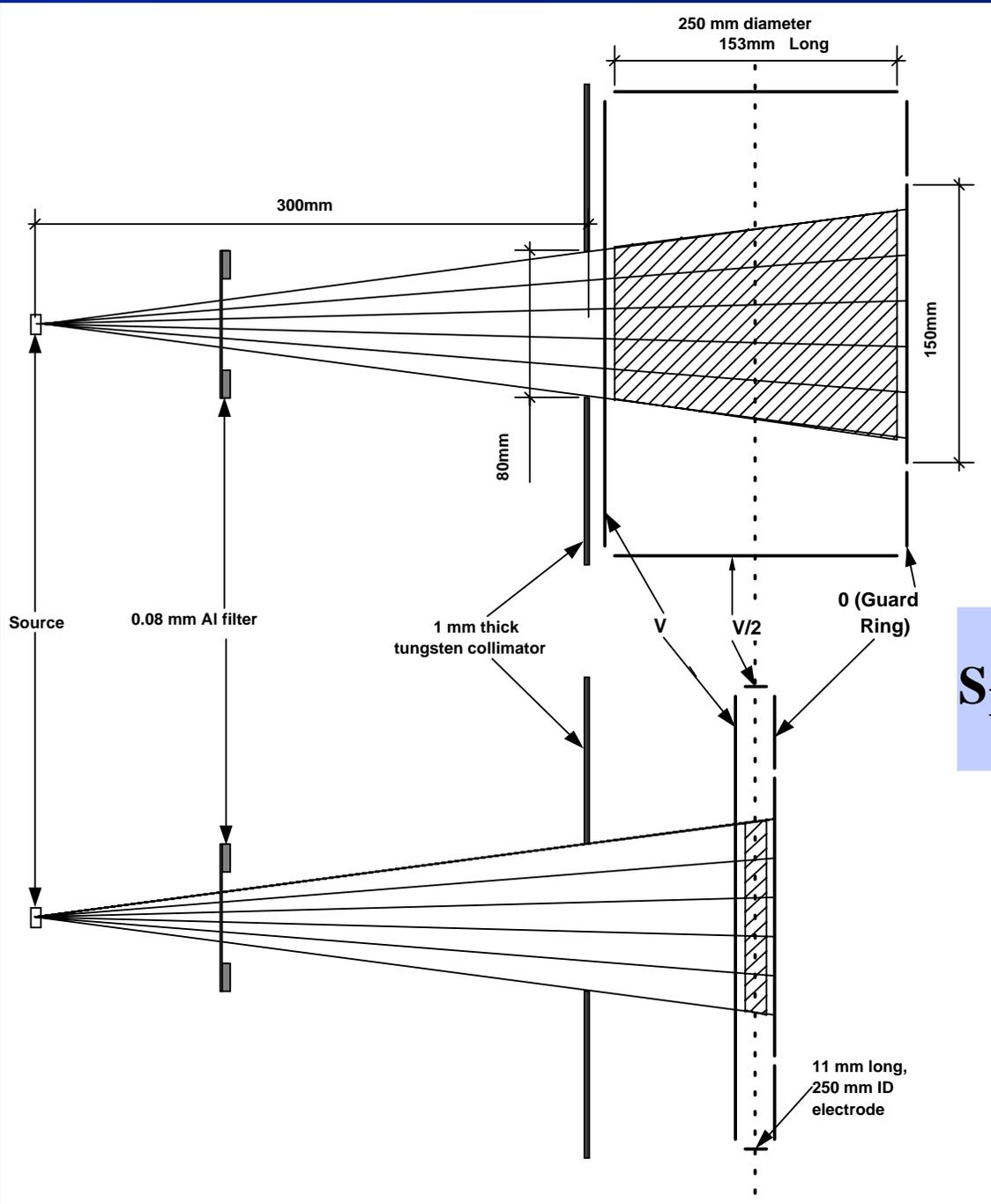
Contact  
Radiograph



Final Model

# Wide-angle Free Air Chamber

NIST Primary Standard  
interstitial sources  
photons < 50 keV



$$S_{K,99N} = \frac{(I_{153} - I_{11})d^2}{\rho_{\text{air}}(V_{153} - V_{11})} (W/e) \prod_i k_i$$

# Analog and Tracklength Dose Estimation

Need cubic array of voxels:

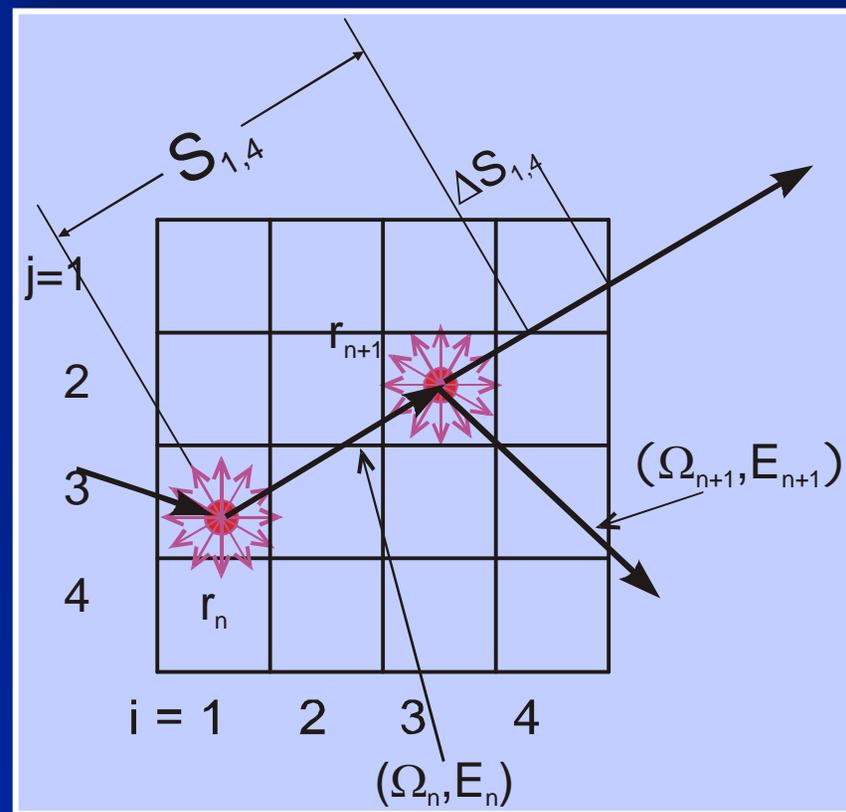
$1 \times 1 \times 1 \text{ mm}^3$  to  $2 \times 2 \times 2 \text{ mm}^3$

Analogue Estimator (EGS method)

$$D_{2,3} \text{ from } n+1 = \frac{\text{Energy in} - \text{Energy out}}{\text{voxel mass}}$$

Expected Value Tracklength Estimator

$$D_{1,4} \text{ from } n \propto E_n \cdot \frac{\Delta S_{1,4}}{\text{voxel volume}} \cdot (\mu_{\text{en}}/\rho)$$



# Estimator Use

- **Tracklength estimators**
  - 20-50X more efficient than analog
  - Models volume averaging and medium replacement by extended detectors
  - 3D patient (voxel array) calculations
- **Next flight estimators: dose-at-a-point**
  - Condensed-medium dose calculations at least 1-2 mm from interfaces
  - Dilute-medium (air) kerma calculations
  - 0.1% - 2% statistical precision for I-125 dosimetry
- **Kalli/Cashwell “Once-more-collided Flux”**
  - Point doses near media interfaces
  - Energy imparted to small detectors

# Monte Carlo quantities for typical seed study

$\Delta D_{\text{wat}}$  (cGy/simulated photon):  $\left\{ \begin{array}{l} \text{Transverse axis} \\ \text{angular dose profiles} \end{array} \right.$

**Bounded next-flight estimator for most distances**

$\Delta E_{\text{ab}}$  Energy imparted to WAFAC volume/simulated photon

**Track-length estimator when fluence varies over detector**

**Next-flight point dose estimator for TLD/diode detectors**

**> 2 cm from source**

$\Delta K_{\text{air}}$  at geometric points  $\left\{ \begin{array}{l} \text{Transverse-axis} \\ \text{in free air} \quad \text{angular fluence profile (30 cm)} \end{array} \right.$

**Track length for WAFAC**

**Next-flight for transverse axis distribution**

# Calculation of TG-43 Parameters by MCPT

MCPT calculates per disintegration within source:

- Dose to medium,  $\Delta D_{\text{med}}(\mathbf{r})$ , near source in phantom geometry: usually 30 cm liquid water sphere
- Air-kerma strength,  $\Delta S_K$ , in free-air geometry usually 5 m air sphere or detailed model of calibration vault

$$\Lambda = \frac{\Delta D_{\text{wat}}(\mathbf{r} = 1 \text{ cm}, \theta = \pi / 2)}{\Delta S_K}$$

$$g(\mathbf{r}) = \frac{\Delta D_{\text{wat}}(\mathbf{r}, \pi / 2) \cdot G(1 \text{ cm}, \pi / 2)}{\Delta D_{\text{wat}}(1 \text{ cm}, \pi / 2) \cdot G(\mathbf{r}, \pi / 2)}$$

## Calculation of $\Delta S_K$ Extrapolated Point-Kerma method

- Place sealed source model at center of large air sphere
- Calculate air-kerma/disintegration,  $\Delta K_{\text{air}}(d)$ , as function transverse axis distance,  $d$
- Extrapolate to free-space geometry by curve fitting

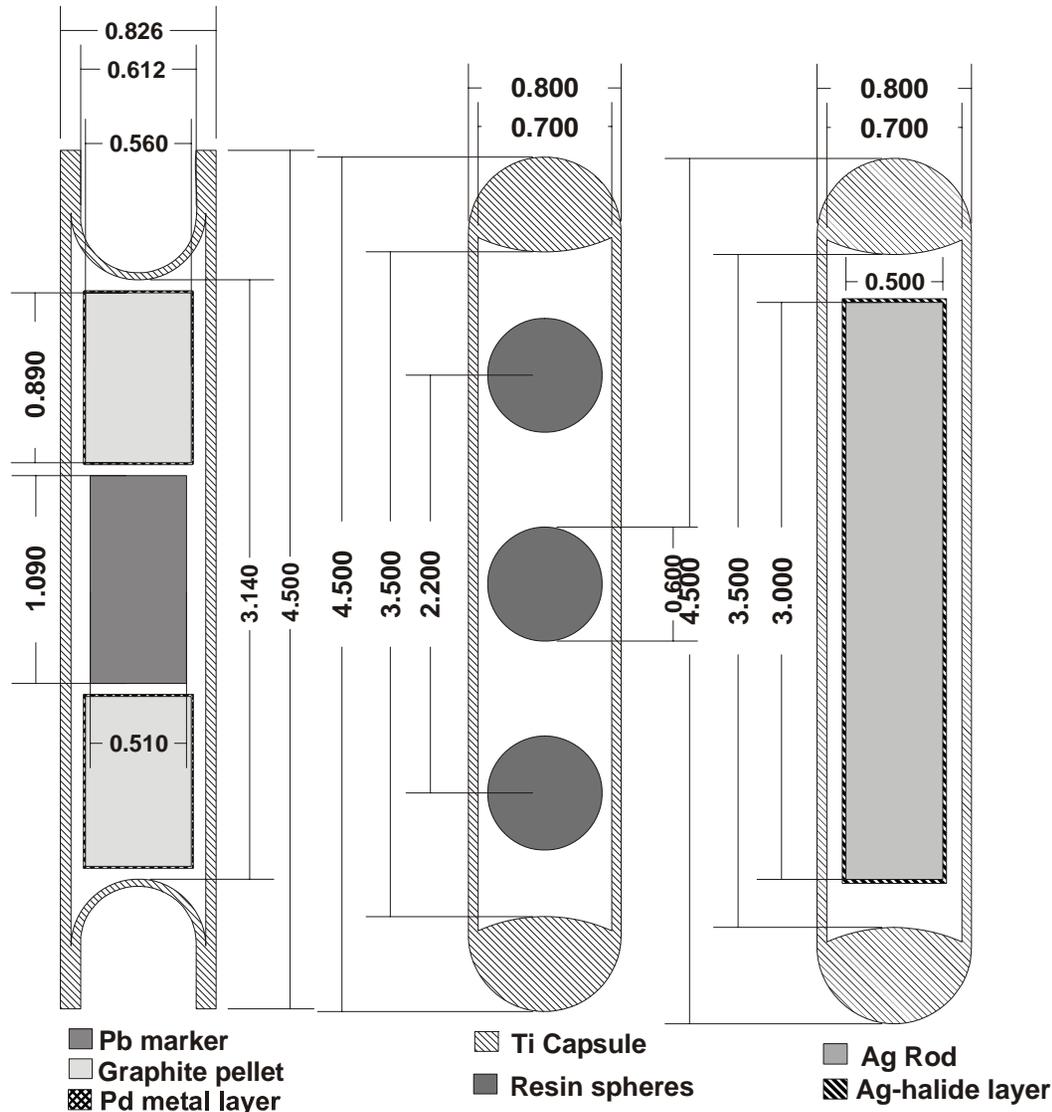
$$\Delta \dot{K}_{\text{air}}(d) \cdot d^2 = \Delta S_K \cdot (1 + \alpha d) \cdot e^{-\mu d}$$

Where  $\Delta S_K$  and  $\alpha$  are unknowns

$(1 + \alpha d)$  - SPR accounts for scatter buildup

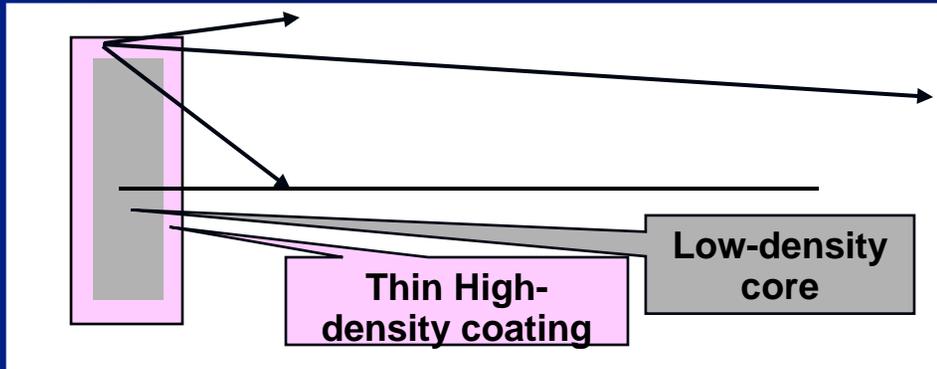
$\mu$  = primary photon attenuation coefficient

# Models 200 ( $^{103}\text{Pd}$ ), 6702 ( $^{125}\text{I}$ ) and 6711 ( $^{125}\text{I}$ ) Seeds

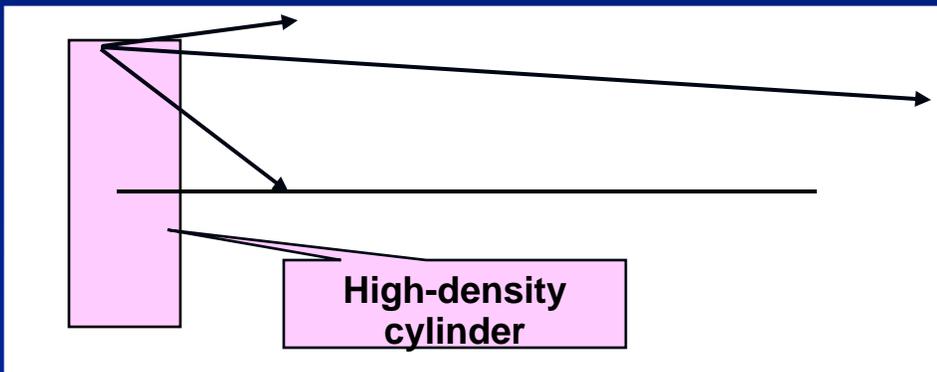


- **Model 200**
  - $^{103}\text{Pd}$  distributed in thin (2-25  $\mu\text{m}$ ) Pd metal coating of right circular graphite cylinder
- **Model 6702**
  - $^{125}\text{I}$  distributed on surface of radio transparent resin spheres
- **Model 6711**
  - $^{125}\text{I}$  distributed in thin ( $\approx 3 \mu\text{m}$ ) silver-halide coating of right circular Ag cylinder

# Sharp corners and opaque coatings

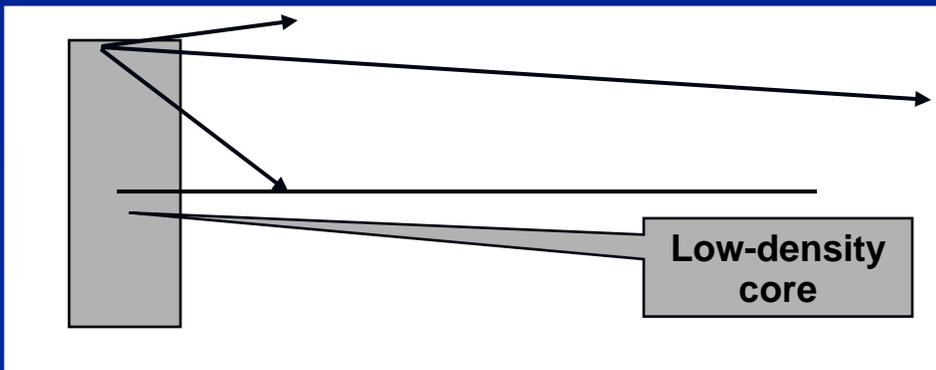


Near transverse-axis:  
Anisotropic at long distances  
Isotropic at short distances  
Inverse square-law deviations



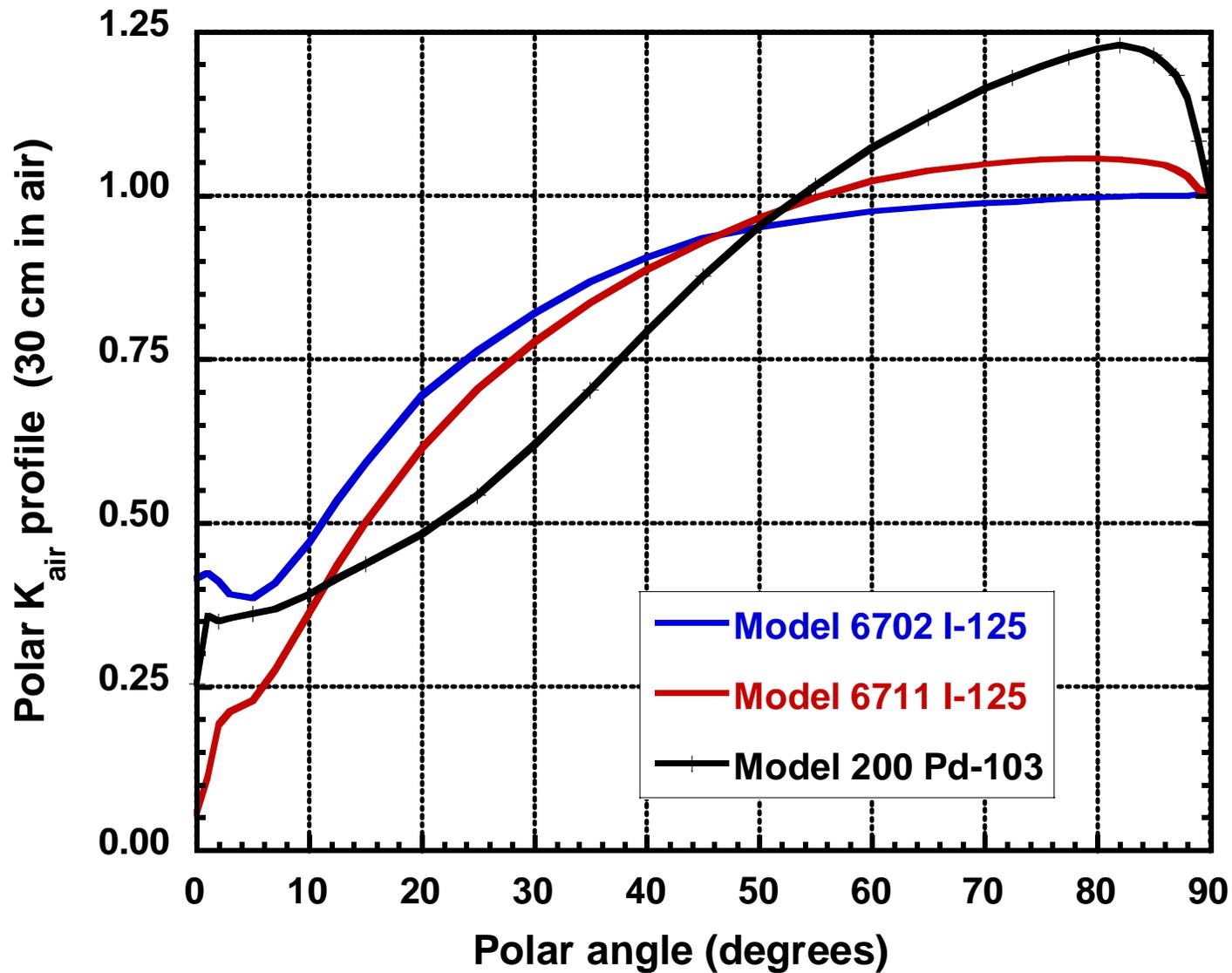
Anisotropic at long and short distances  
Circular ends contribute at

$$\theta = \tan^{-1} \left[ \frac{L}{2 \times d} \right] = \begin{cases} 8^\circ & d = 1 \text{ cm} \\ 0.3^\circ & d = 30 \text{ cm} \end{cases}$$

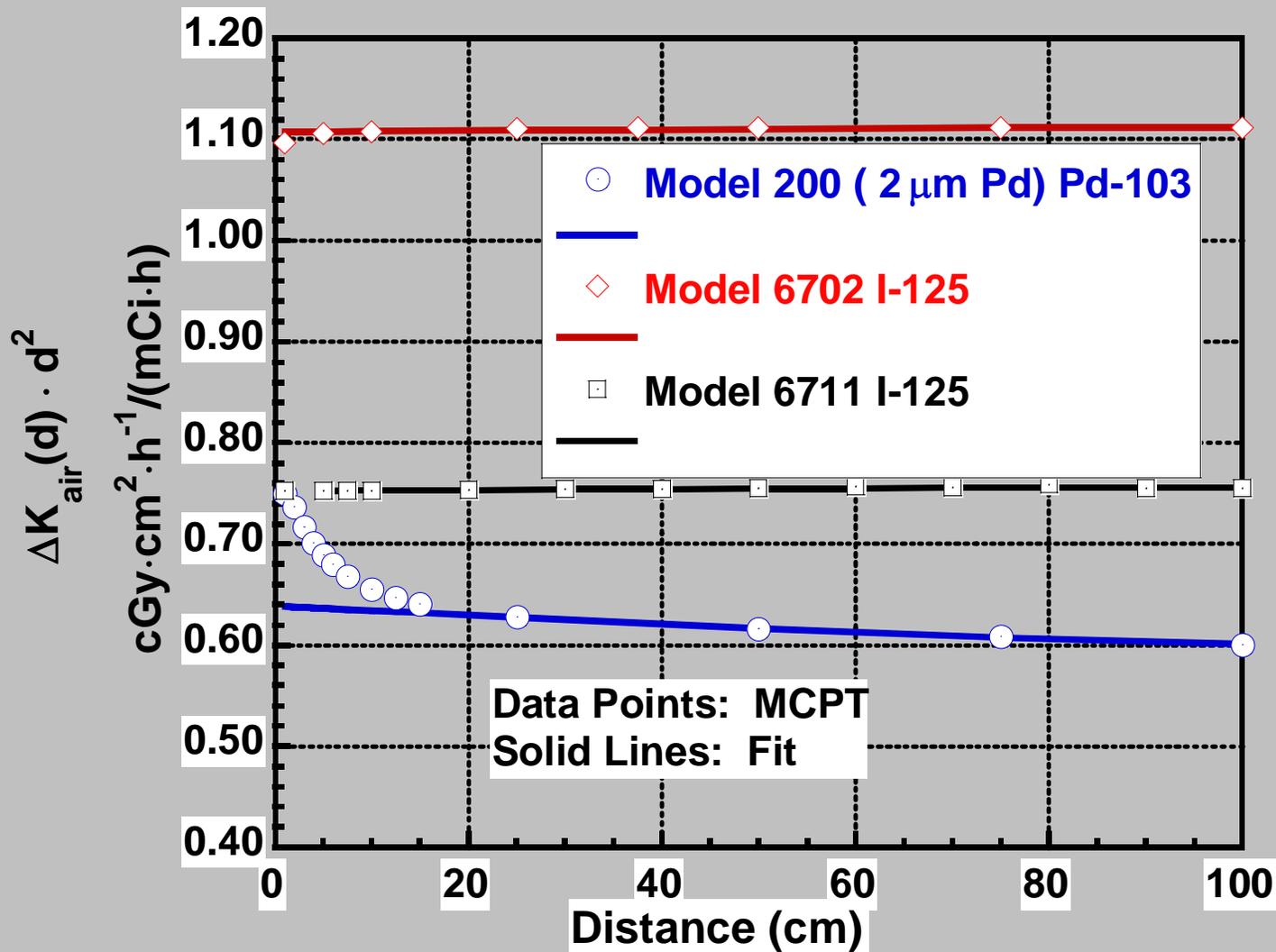


Isotropic at both long and short distances

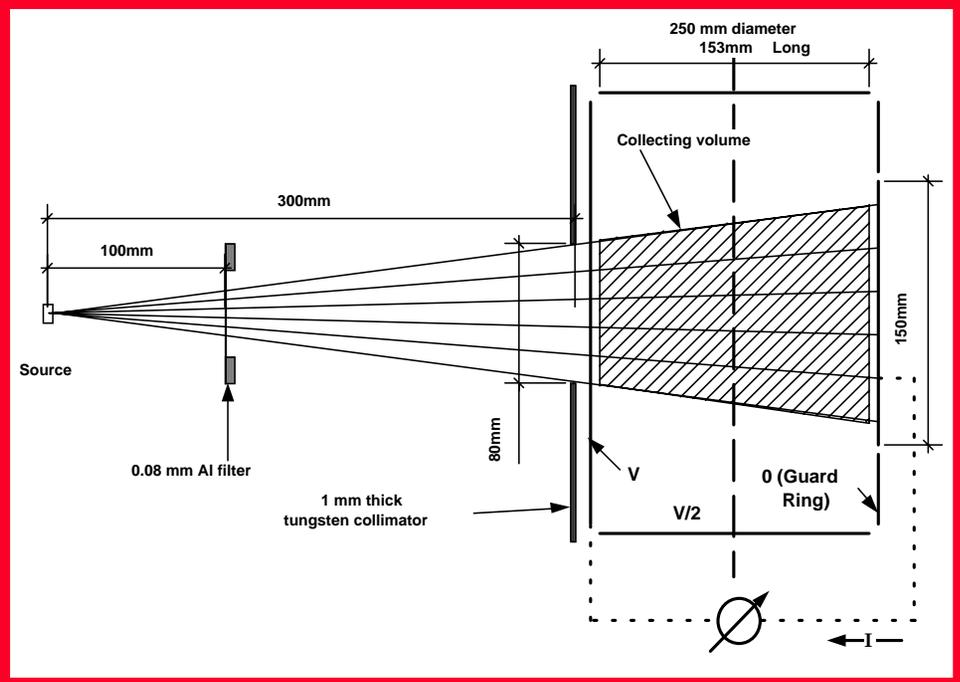
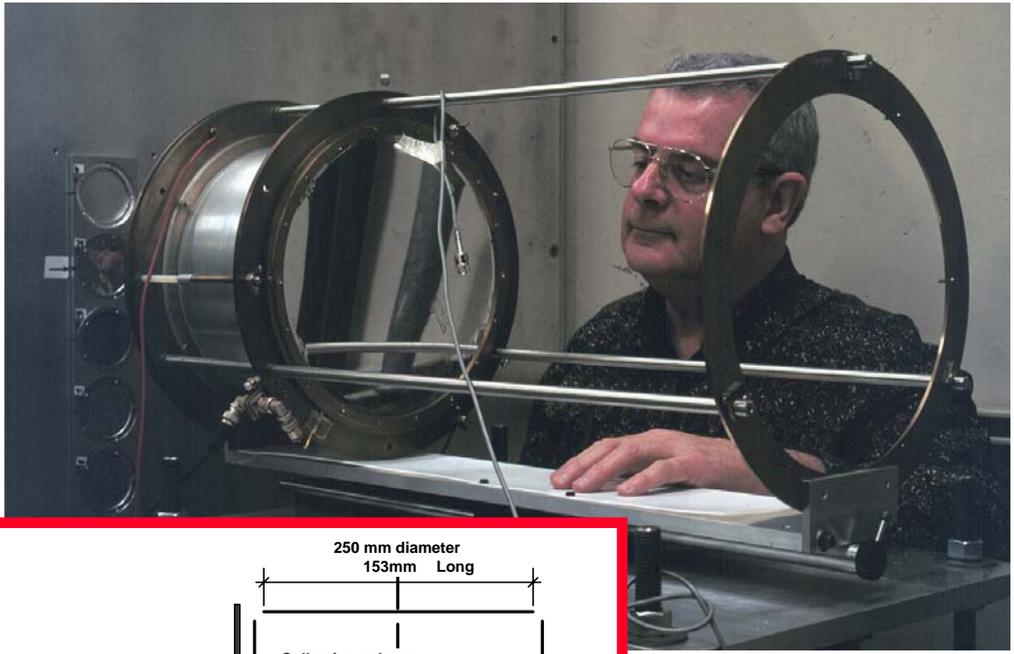
# Polar Anisotropy in Air (30 cm)



# $\Delta S_K$ : Point-Extrapolation Method



# 'WAFAC:' Wide Angle Free-Air Chamber



Rotating Seed Holder

# WAFAC Simulation Method

$$\Delta S_K = \frac{(\Delta E_{ab}^{153} - \Delta E_{ab}^{11}) \cdot d^2}{\rho_{air} \cdot (V_{153} - V_{11})} \cdot k_{inv} \cdot k_{att}$$

where  $\Delta E_{ab}^x$  = Energy absorbed/disintegration in WAFAC volume of length  $x$   
 $d = 38 \text{ cm} = \text{seed-to-WAFAC volume center}$

$$k_{att} = \frac{(\Delta S_K)_{extr}}{k_{inv} \cdot (\Delta K \cdot d^2)_{WFC}} \left. \vphantom{\frac{(\Delta S_K)_{extr}}{k_{inv} \cdot (\Delta K \cdot d^2)_{WFC}}} \right\} \text{for a point source} = \begin{cases} 1.025 & \text{Pd-103} \\ 1.013 & \text{I-125} \end{cases}$$

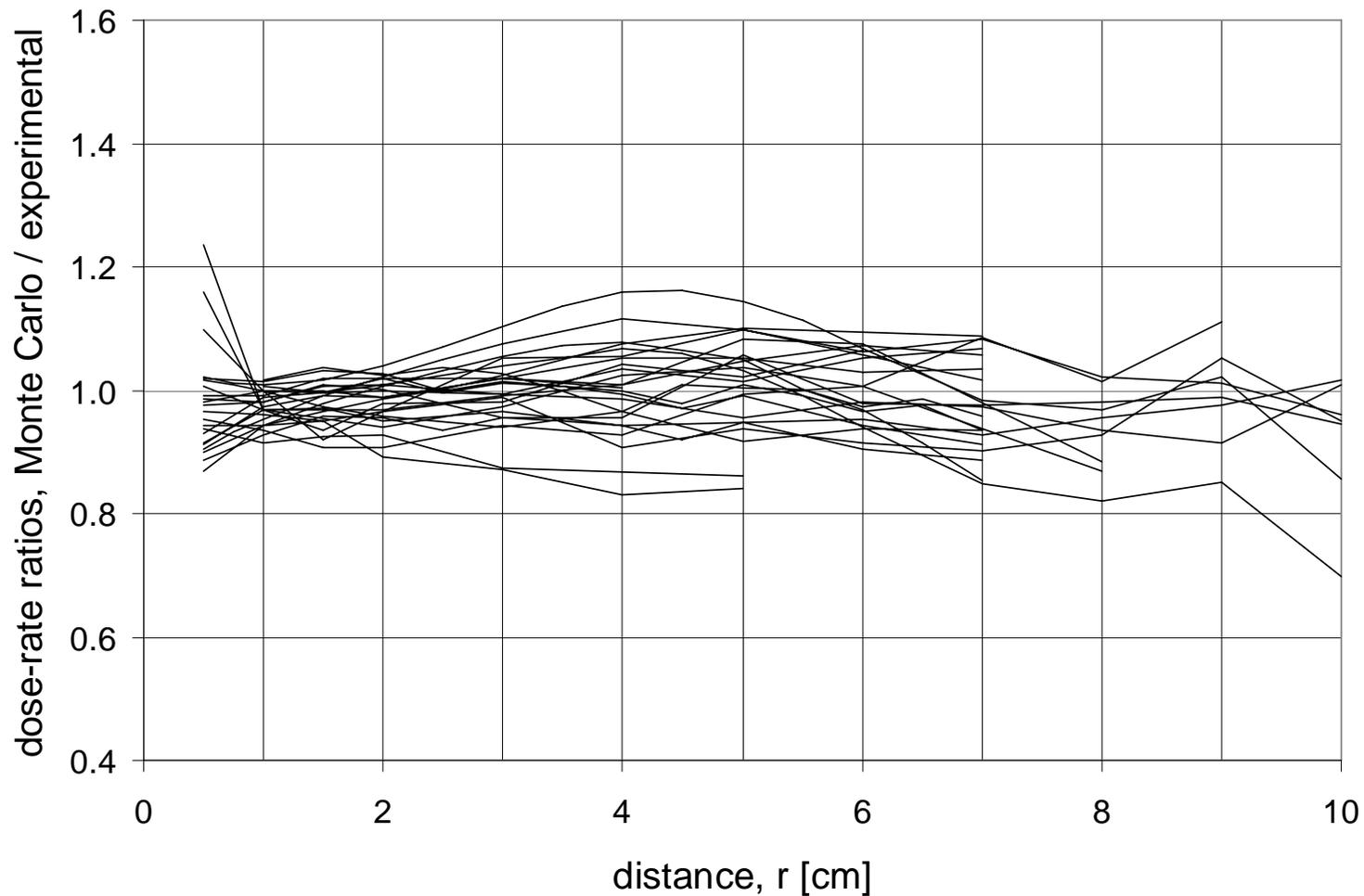
$$k_{inv} = \text{inverse-square correction} = \frac{\int_A \Phi(\ell) \cdot dA}{\Phi(d) \cdot A} = 1.0089$$

# Pd-103 Dose-Rate Constants

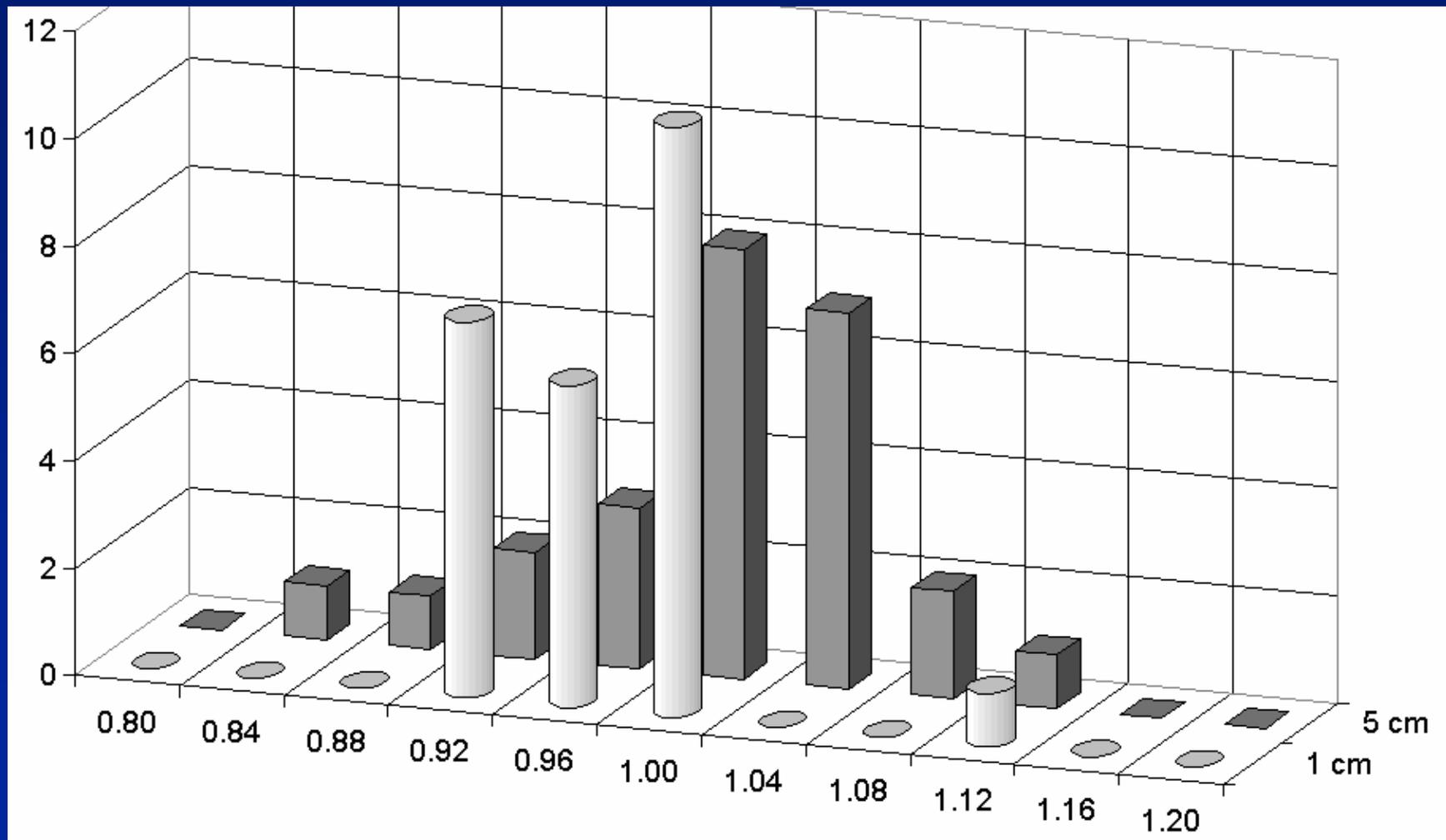
Source	Investigator	$\Lambda_{xxD,N99S}$		
		TLD	MC Extrap.	MC WAFAC
Point	This work	—	0.683	0.683
Model 200 (light)	This work	---	0.797	0.691
	Nath 2000 ICWG 1989	0.684 0.65		
Model 200 (heavy)	This work ICWG 1989	----- 0.65	0.744	0.694
NAS MED 3633	Li Wallace 1998	0.693 0.68	0.677	---

# Monte Carlo vs. TLD: $^{125}\text{I}$ Seeds

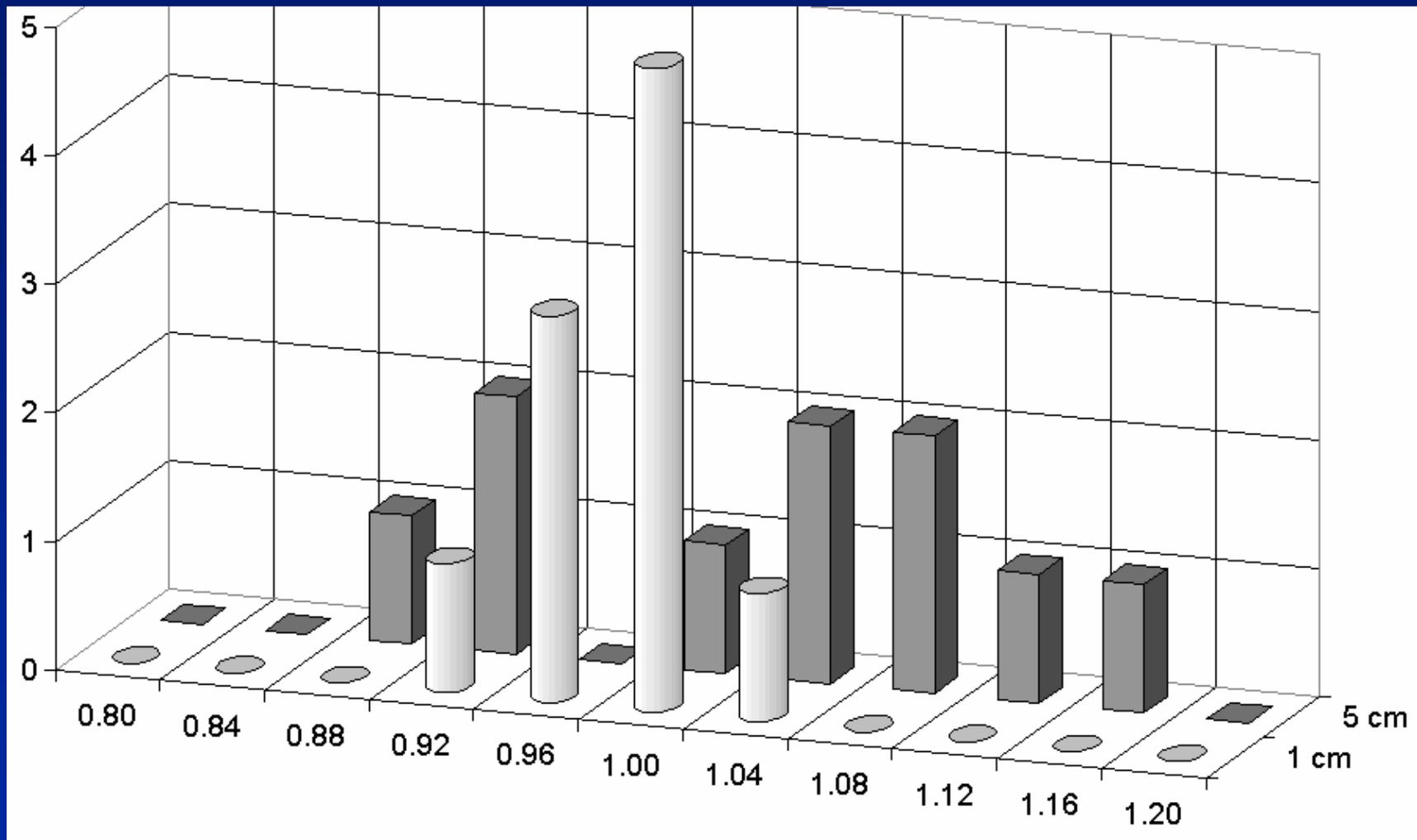
- 14 Seed models, 38 Candidate datasets



# Monte Carlo/TLD Dose Rates: $^{125}\text{I}$ Seeds



# Monte Carlo/TLD Dose Rates: $^{125}\text{I}$ Seeds



# TLD and Monte Carlo Uncertainty Analysis

**Table 2: Uncertainties for  $^{125}\text{I}$  transverse-axis TLD and Monte Carlo dose estimation**

TLD uncertainties in measurement of $\dot{D}_{wat}(\vec{r})/S_K$ for $^{125}\text{I}$ in Solid Water				
Component	1 cm distance		5 cm distance	
	$\% \sigma_x$	Type	$\% \sigma_x$	Type
Repetitive TLD measurements	<b>4%</b>	<b>A</b>	<b>4%</b>	<b>A</b>
TLD calibration (including Linac calibration)	<b>3%</b>	<b>A+B</b>	<b>3%</b>	<b>A+B</b>
Solid-to-liquid water conversion	<b>2%</b>	<b>B</b>	<b>6%</b>	<b>B</b>
Seed and TLD positioning errors ( $\Delta d = 100 \mu\text{m}$ )	<b>2%</b>	<b>B</b>	<b>1%</b>	<b>B</b>
Energy-response correction	<b>5%</b>	<b>B</b>	<b>5%</b>	<b>B</b>
ADCL $S_K$ measurement + transfer	<b>2%</b>	<b>B</b>	<b>2%</b>	<b>B</b>
<b>Total combined uncertainty</b>	<b>7.9%</b>		<b>9.5%</b>	
Uncertainties for Monte Carlo estimates $\dot{D}_{wat}(\vec{r})/S_K$ for $^{125}\text{I}$ in liquid water				
Statistics	<b>0.3%</b>		<b>1.0%</b>	
Photo ionization cross-sections ( $\Delta \sigma_{PE} = 2.3\%$ )	<b>1.5%</b>		<b>4.5%</b>	
Seed geometry	<b>2%</b>		<b>2%</b>	
Source energy spectrum	<b>0.1%</b>		<b>0.3%</b>	
<b>Total combined uncertainty</b>	<b>2.5%</b>		<b>5.0%</b>	

# Monte Carlo vs TLD

- **Measurement Pros and Cons**
  - Large uncertainties and many artifacts
  - Tests conjunction of all a priori assumptions: seed geometry, detector response corrections, etc
- **Monte Carlo Pros and Cons**
  - Artifact free and low uncertainty
  - Garbage in-Garbage out
    - » Seed geometry errors
    - » Will not anticipate contaminant radionuclides etc.,  $S_K$  errors
  - Does not model detector signal formation

# Conclusions

- **Low energy brachytherapy: main catalyst for improving dosimetry and source standardization for 30 years**
  - Single-source dose distributions have 5% uncertainty
  - Both MC and measurement have important roles
- **Current Role**
  - Monte Carlo: primary source of dosimetric data
  - Measurement: Confirm assumptions underlying Monte Carlo model
- **Major needs: more accurate and efficient dose-measurement systems for low energy sources**
  - Test source-to-source variations during manufacturing process